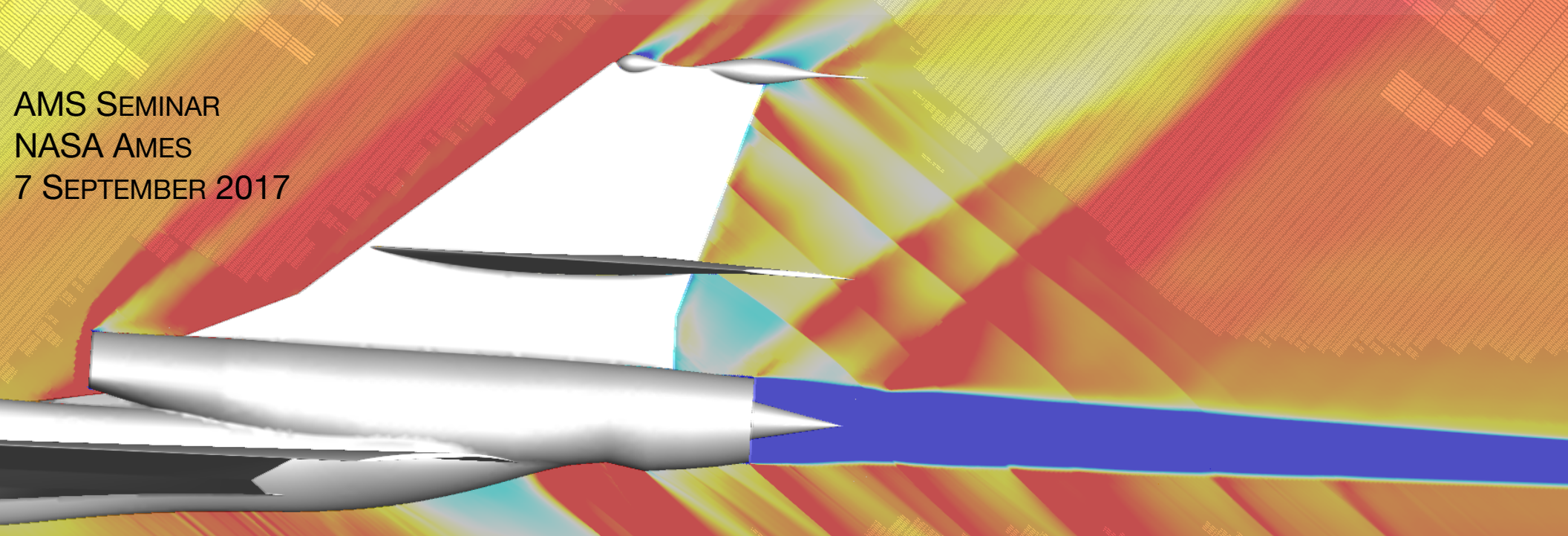


CART3D SIMULATIONS

FOR THE 2ND AIAA SONIC BOOM PREDICTION WORKSHOP

AMS SEMINAR
NASA AMES
7 SEPTEMBER 2017



George R. Anderson

Science & Technology Corp.

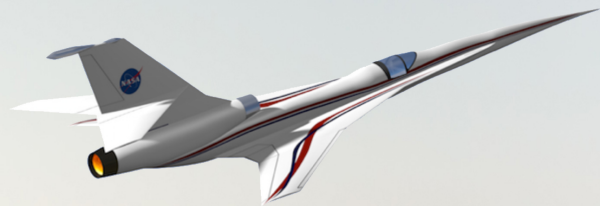
Michael J. Aftosmis

NASA Ames

Marian Nemec

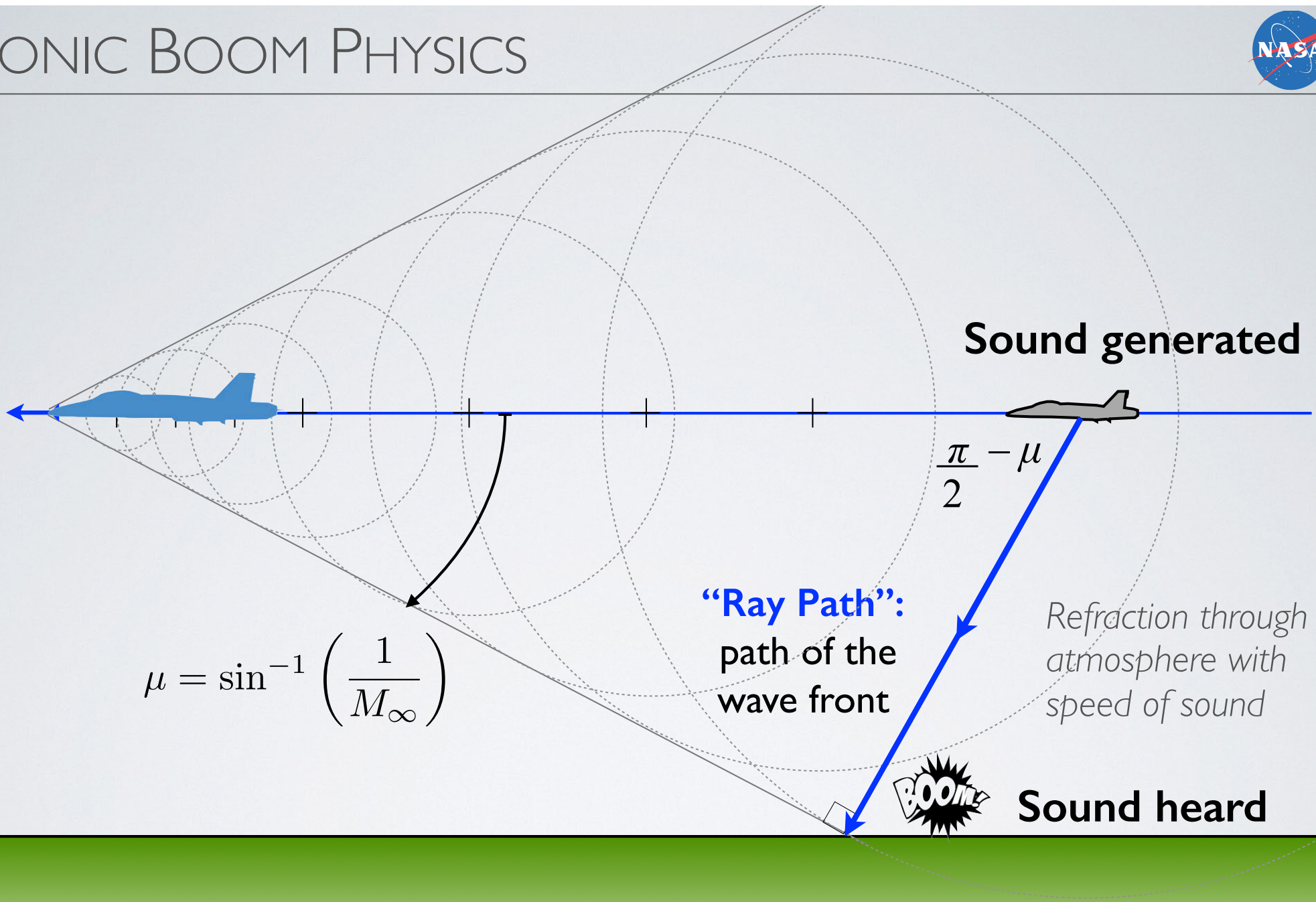
NASA Ames

Computational Aerosciences Branch
NASA ARC — Moffett Field, CA

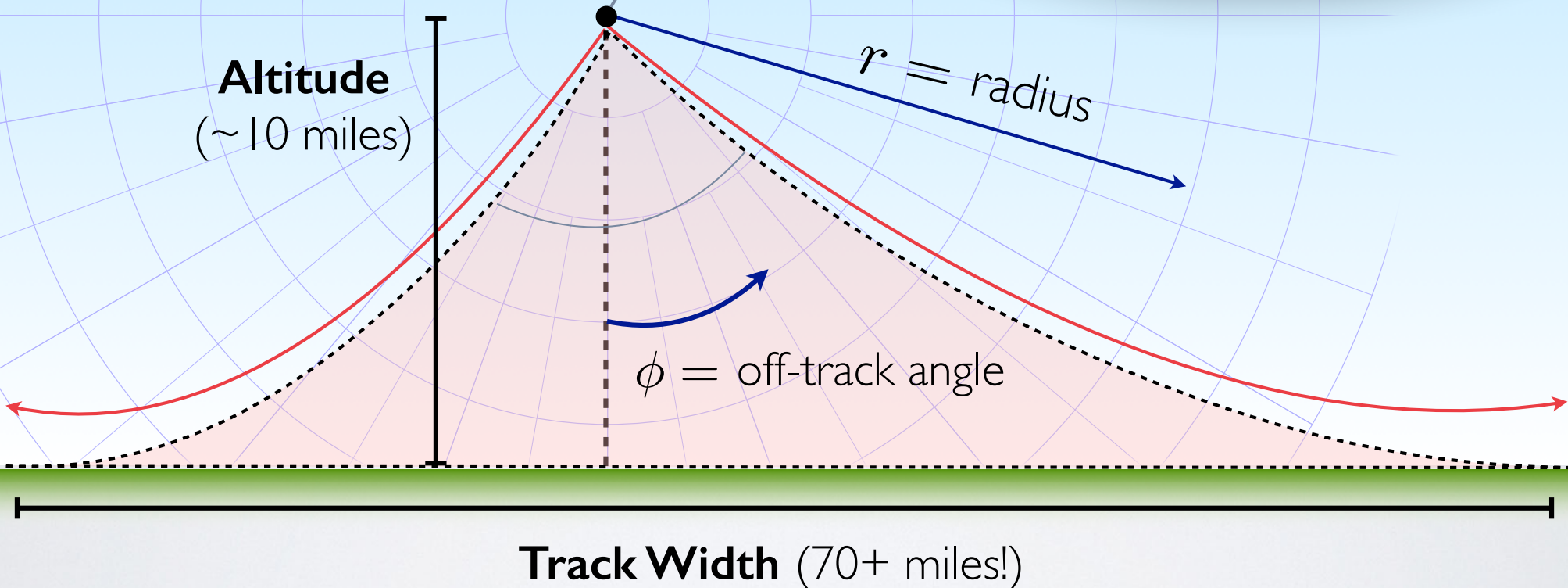
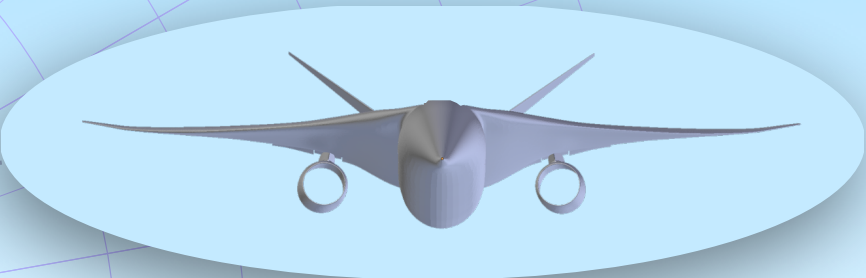


- **Commercial supersonic flight** banned over the US because of objectionable sonic boom
- Hope to overturn this with demonstrably quiet aircraft (e.g. QueSST/LBFD)
- **CFD tools are a major contributor to design efforts**
- Sonic Boom Prediction Workshops
 - (2008) NASA FAP SBPW
 - (2014) AIAA SBPW I
 - **(2017) AIAA SBPW2**

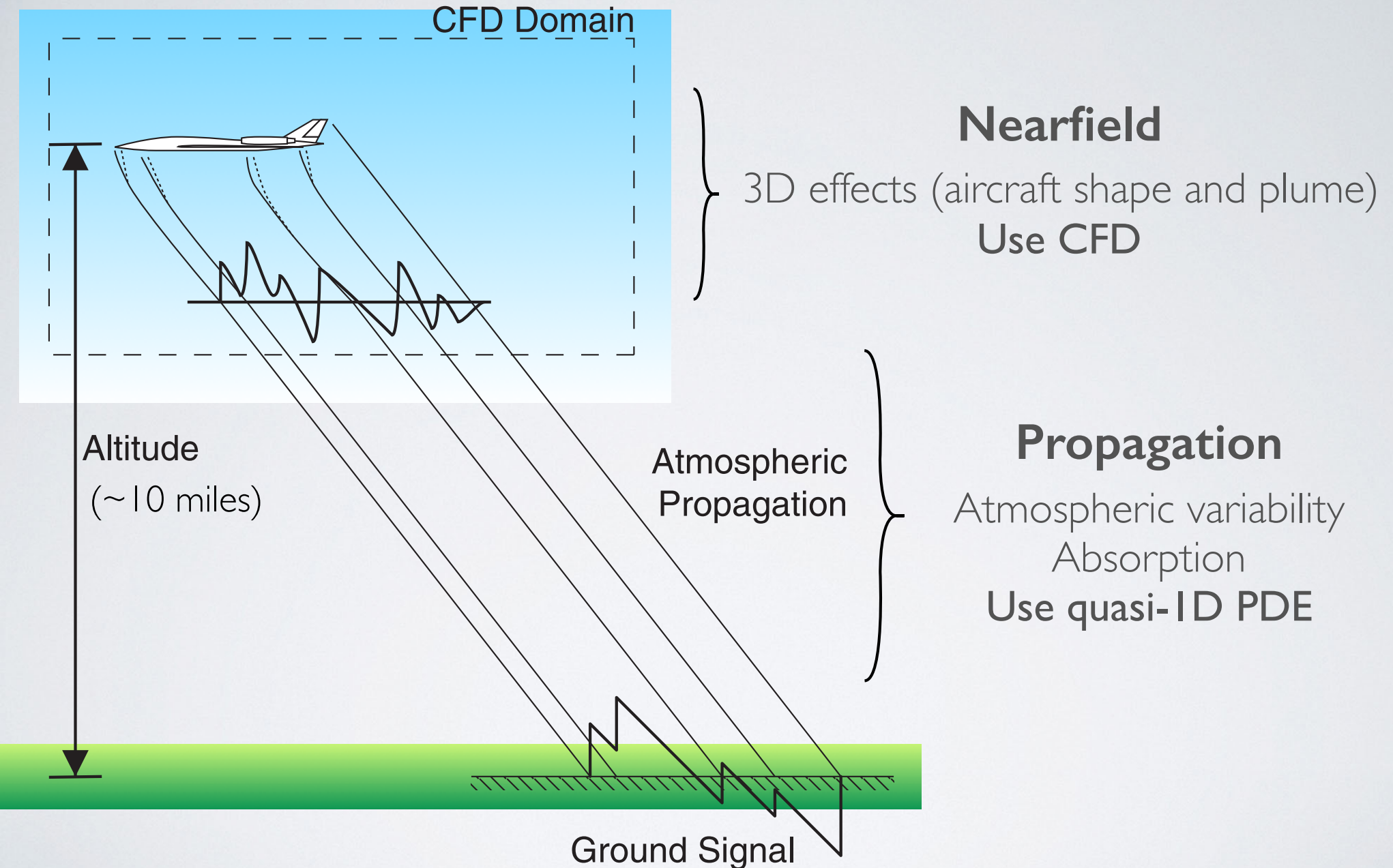
SONIC BOOM PHYSICS



BOOM CARPETS



SONIC BOOM PREDICTION



- Workshop Results
- Nearfield (2/4 cases)
- Propagation
- Full Vehicle-to-Boom Simulation Path
- Conclusions

AIAA PAPER 2017-3255

Cart3D Simulations for the Second AIAA Sonic Boom Prediction Workshop

George R. Anderson*
Science and Technology Corporation, Moffett Field, CA 94035
 Michael J. Aftosis† and Marian Nemeč‡
NASA Ames Research Center, Moffett Field, CA 94035

Simulation results are presented for all test cases prescribed in the Second AIAA Sonic Boom Prediction Workshop. For each of the four nearfield test cases, we compute pressure signatures at specified distances and off-track angles, using an inviscid, embedded-boundary Cartesian-mesh flow solver with output-based mesh adaptation. The cases range in complexity from an axisymmetric body to a full low-boom aircraft configuration with a powered nacelle. For efficiency, boom carpets are decomposed into sets of independent meshes and computed in parallel. This also facilitates the use of more effective meshing strategies — each off-track angle is computed on a mesh with good azimuthal alignment, higher aspect ratio cells, and more tailored adaptation. The nearfield signatures generally exhibit good convergence with mesh refinement. We introduce a local error estimation procedure to highlight regions of the signatures most sensitive to mesh refinement. Results are also presented for the two propagation test cases, which investigate the effects of atmospheric profiles on ground noise. Propagation is handled with an augmented Burgers' equation method (NASA's sBOOM), and ground noise metrics are computed with LCASB.

Nomenclature

A_{ref}	Reference area	Φ	Off-track/Azimuthal angle
$C_{D/L/M}$	Drag/lift/pitching moment coefficients		<i>Subscripts</i>
C_p	Local pressure coefficient	$(\cdot)_{\infty}$	Freestream value
e	Integrated signature differences	$(\cdot)_f$	Stagnation value
E	Local error estimate	$(\cdot)_c$	Coarse
J	Aerodynamic output functional	$(\cdot)_f$	Fine
l	Distance along signature	$(\cdot)_m$	Medium
L	Reference length for propagation		
M	Mach number		<i>Abbreviations</i>
p	Static pressure		ABEL/CSEL A-/C-weighted sound exposure level
ρ	Order of convergence		AXIE Axisymmetric body (Case I)
r	Distance from flight path		AXIE-PREP Axisymmetric body (Prop. Case I)
T	Temperature		C25P C25b with flow-through nacelle (Case III)
w	Weight in functional		C25P C25b with powered nacelle (Case IV)
α	Angle of attack		JWB JAXA wing-body (Case II)
β	$\sqrt{M_{\infty}^2 - 1}$		LCASB Loudness Code for Asymmetric Sonic Booms
θ	Offset angle to avoid sonic glitch		LM-102 Lockheed Martin 1021 (Prop. Case II)
μ	Mach angle = $\sin^{-1}(1/M_{\infty})$		PL Perceived level of noise
ρ	Density		SBPW Sonic Boom Prediction Workshop
τ	Normalized z-distance from nose Mach cone		

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 †Aerospace Engineer, Computational Aerodynamics Branch, michael.aftosis@nasa.gov, Associate Fellow AIAA.
 ‡Aerospace Engineer, Computational Aerodynamics Branch, marian.nemec@nasa.gov, Member AIAA.

ALL REQUIRED AND OPTIONAL
 CASES FROM BOTH WORKSHOPS

NEARFIELD CASES

AXIE

JWB

C25F

C25P

Today

ALL CASES:
MACH 1.6
Altitude: 15.76 km
(~52K feet)

▶ **Nearfield Workshop — Cart3D**

- **Meshing approach** — Mach Alignment + Adaptation
 - **Boom Carpets** — Azimuthal Alignment
 - **Results** for Cases 1 and 4
 - **Local Error Analysis**
-
- Propagation Workshop
 - Full Vehicle-to-Boom Simulation Path
 - Conclusions

CFD AND MESHING

Flow Solver — Cart3D v1.5

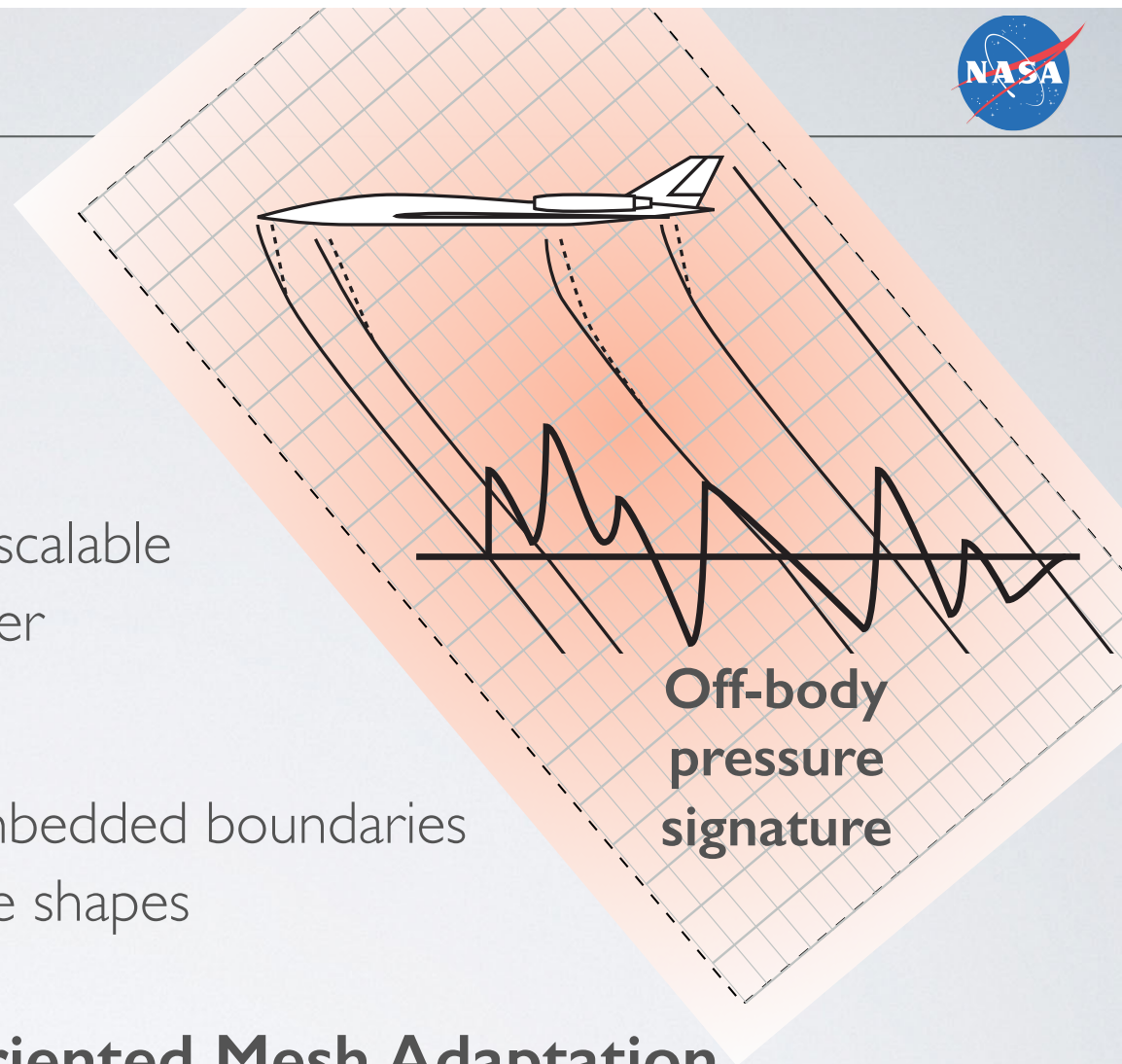
- ▶ Steady, inviscid flow
- ▶ 2nd-order upwind method
- ▶ Multigrid acceleration
- ▶ Domain decomposition — highly scalable
- ▶ *For this work:* Barth-Jespersen limiter

Automatic Meshing

- ▶ Multilevel Cartesian mesh with embedded boundaries
- ▶ Handles arbitrarily complex vehicle shapes

Error Estimation and Goal-Oriented Mesh Adaptation

- ▶ Discretization error estimates computed via method of adjoint-weighted residuals
- ▶ Mesh automatically refined in locations with most impact on signatures



**Off-body
pressure
signature**

MESHING

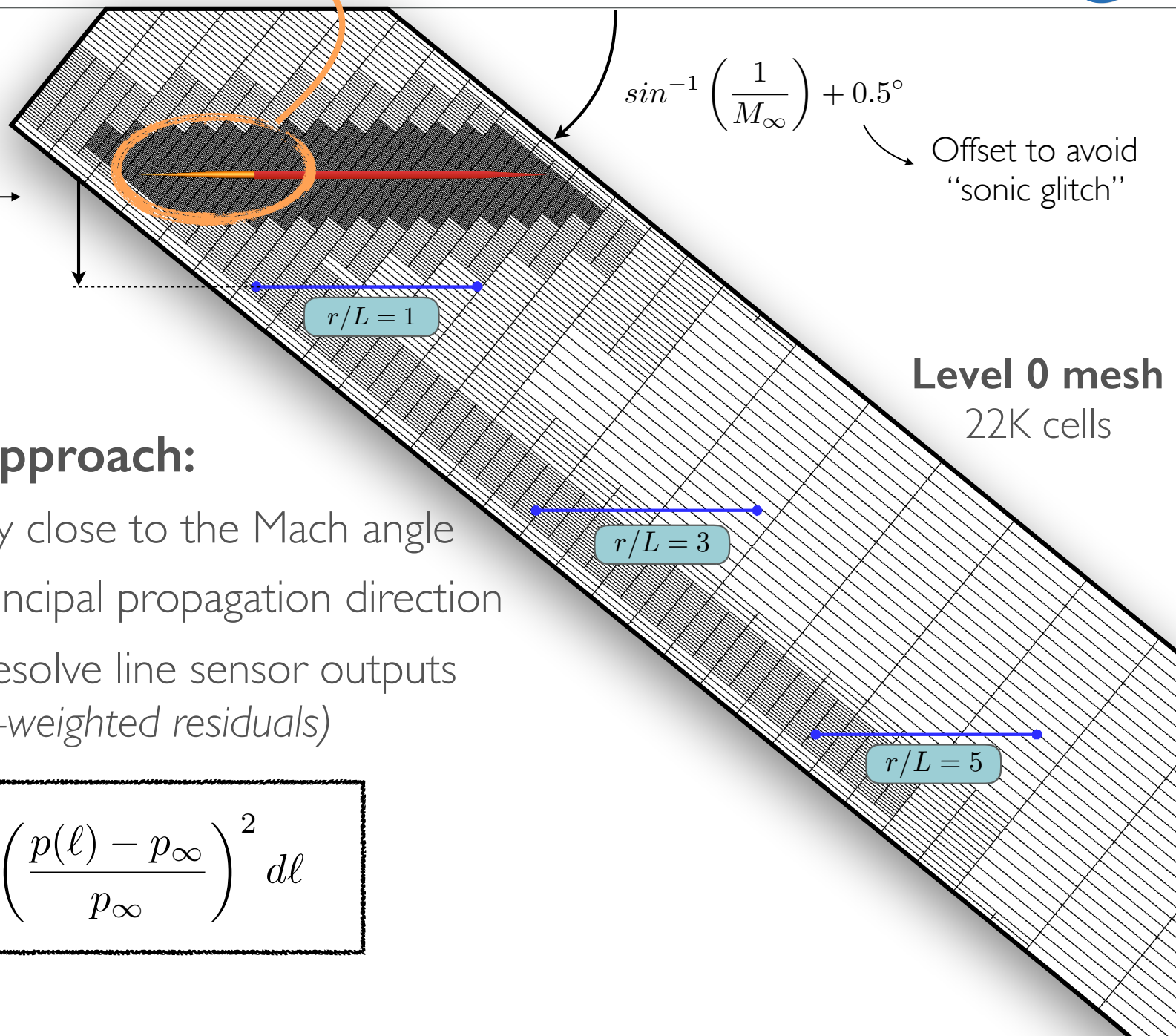


AXIE

$M_\infty = 1.6$
 $\alpha = 0^\circ$

$$\sin^{-1} \left(\frac{1}{M_\infty} \right) + 0.5^\circ$$

Offset to avoid "sonic glitch"



Level 0 mesh
22K cells

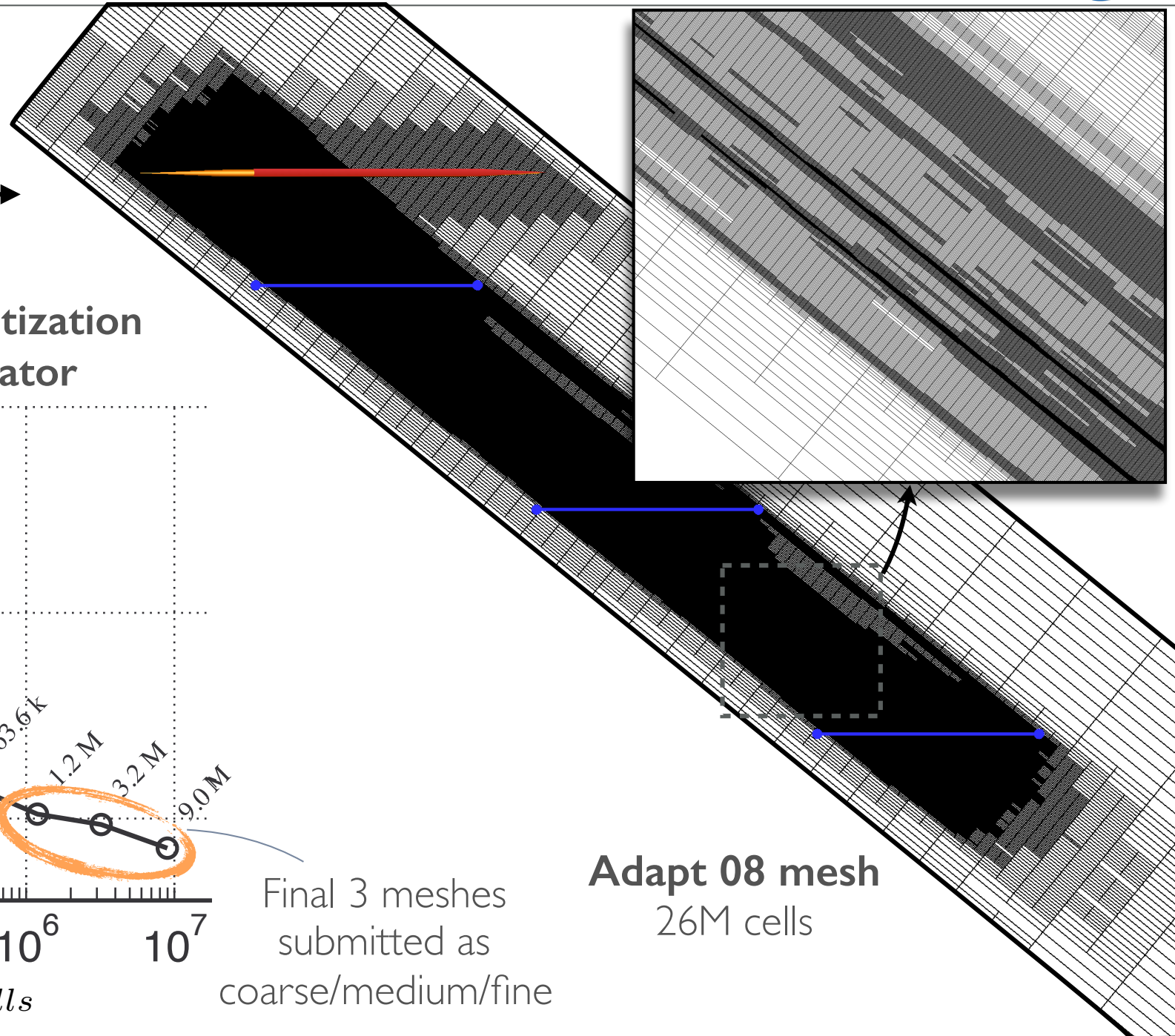
Basic Meshing Approach:

1. **Rotate** mesh very close to the Mach angle
2. **Stretch** in the principal propagation direction
3. **Adapt** mesh to resolve line sensor outputs
(method of adjoint-weighted residuals)

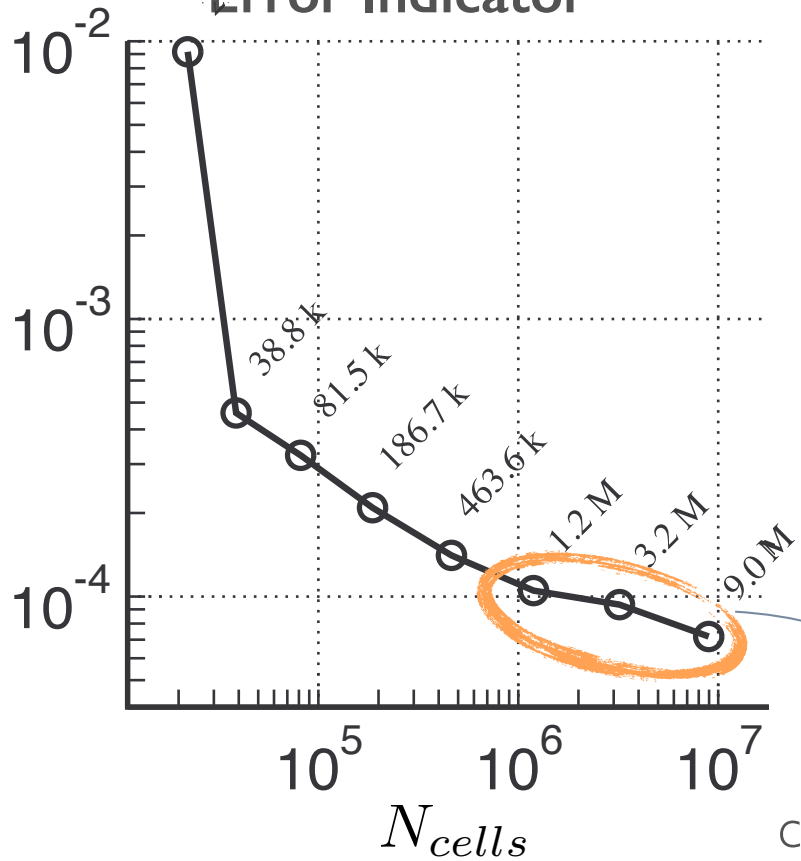
$$\mathcal{J}_r = \int_0^L w(\ell) \left(\frac{p(\ell) - p_\infty}{p_\infty} \right)^2 d\ell$$

ADAPTATION

$M_\infty = 1.6$
 $\alpha = 0^\circ$



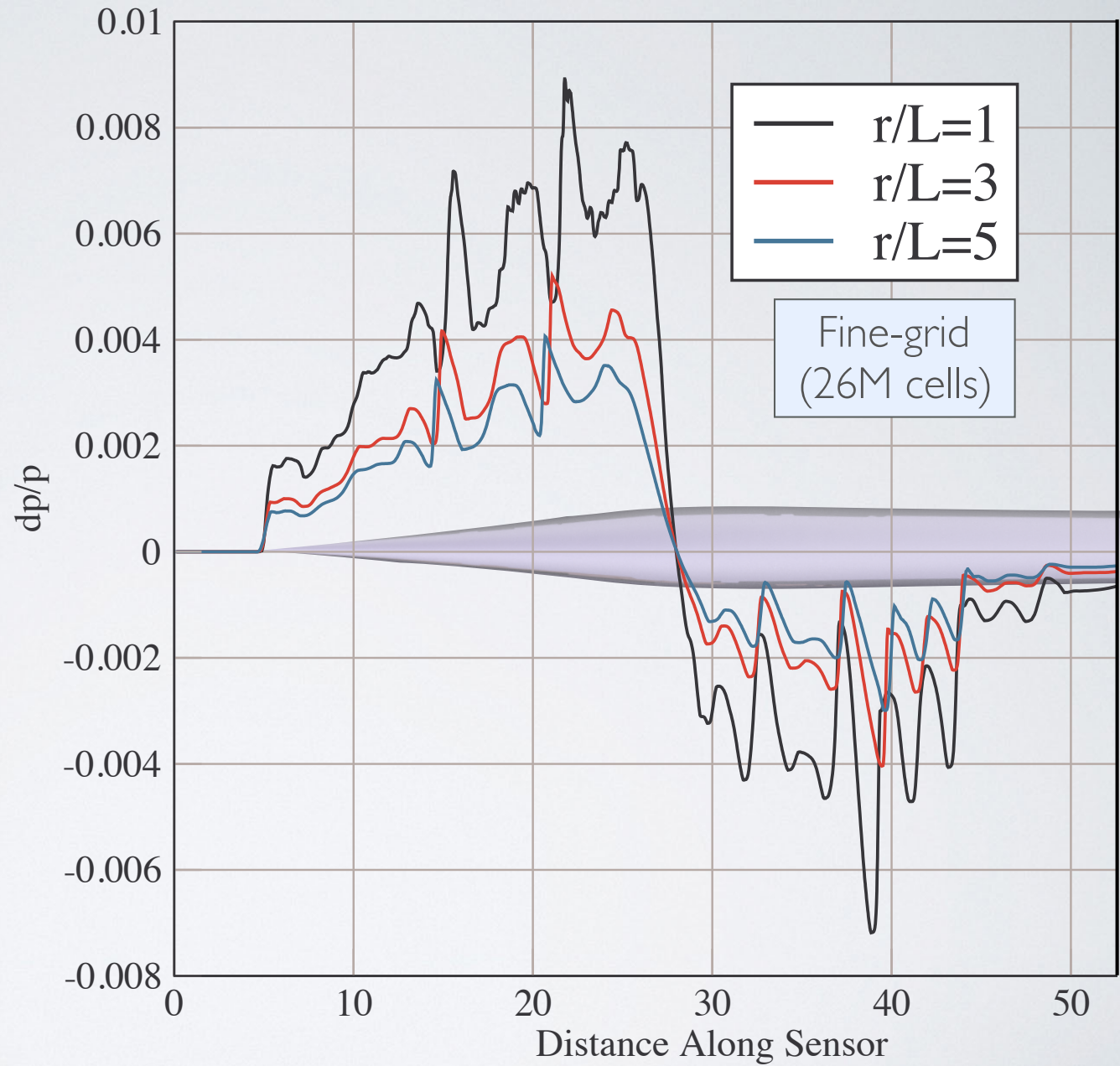
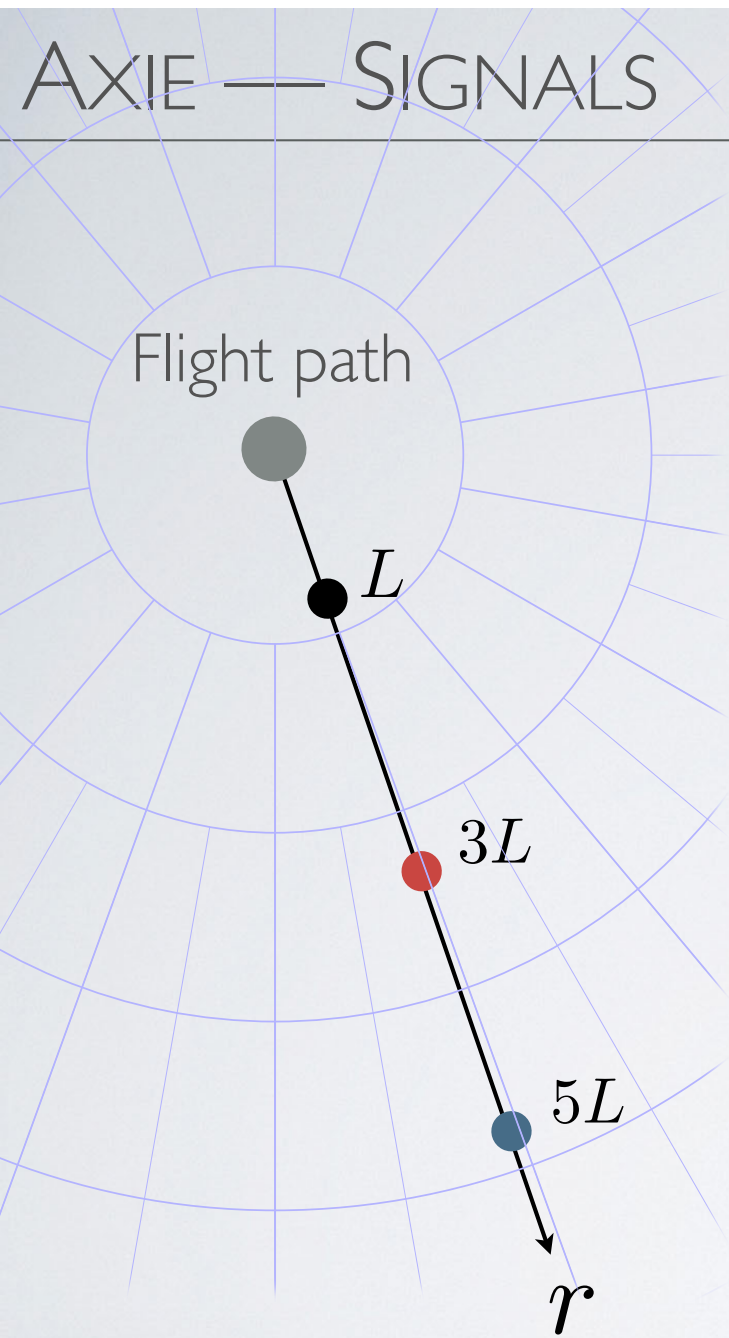
Adjoint Discretization Error Indicator



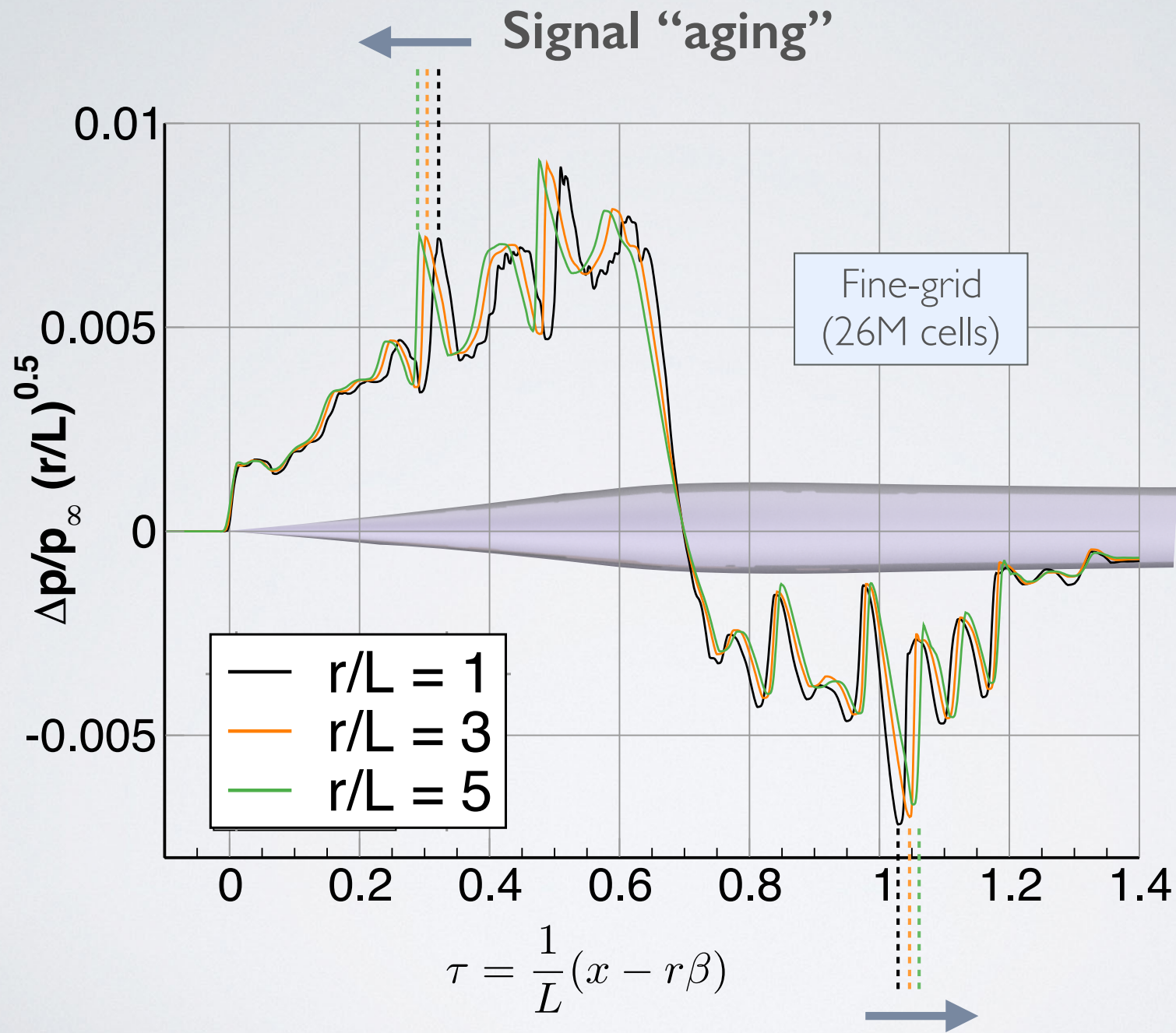
Final 3 meshes submitted as coarse/medium/fine

Adapt 08 mesh
26M cells

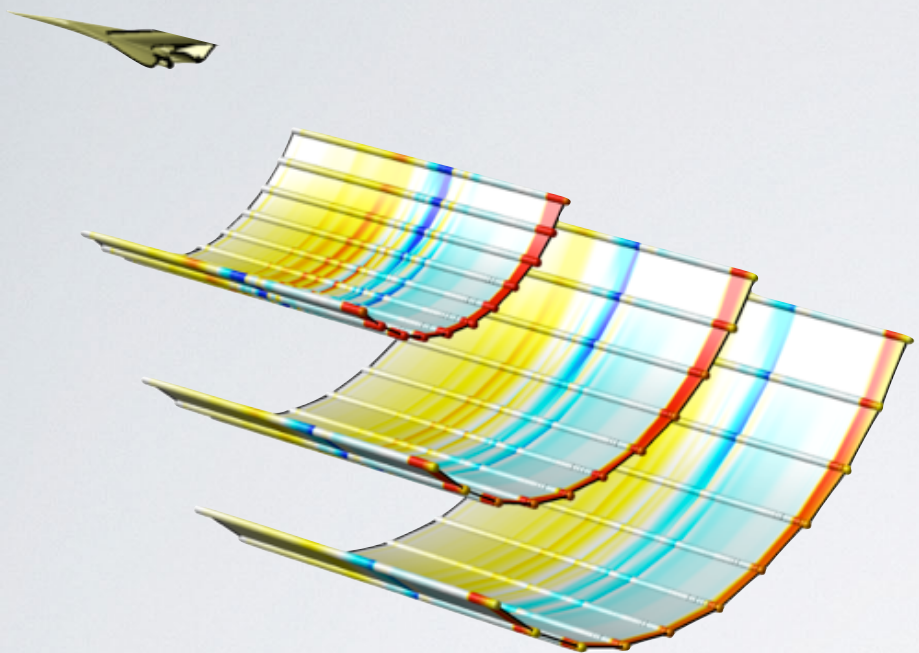
AXIE — SIGNALS



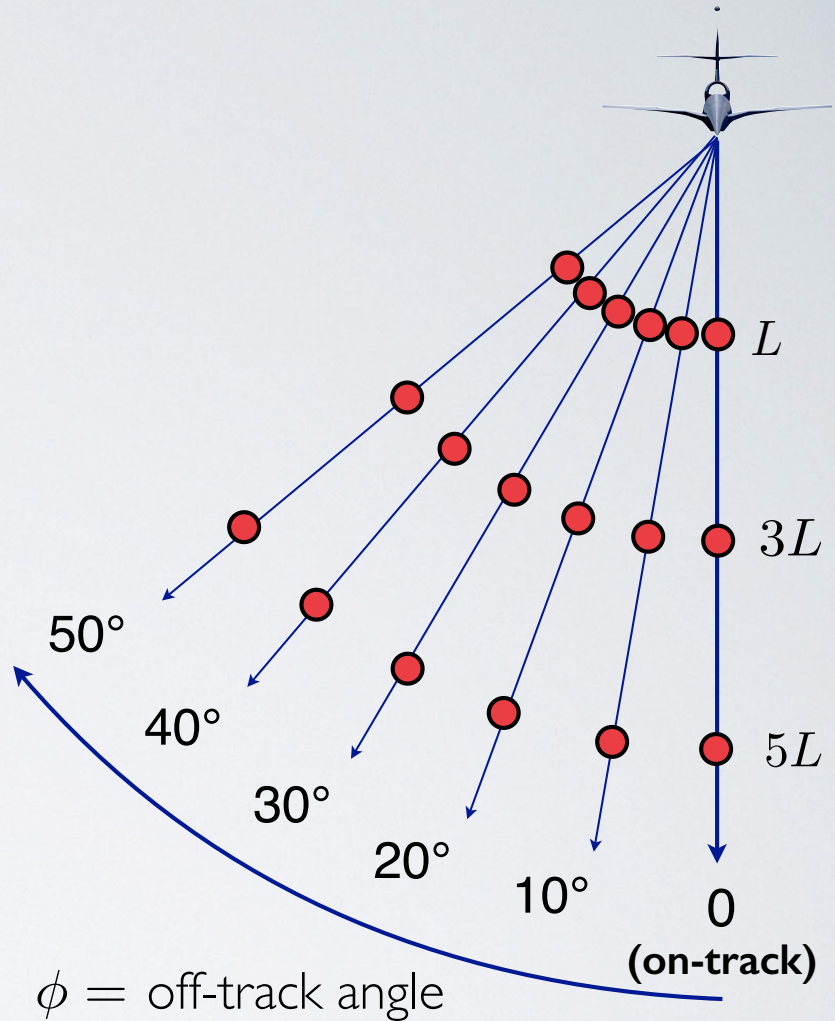
AXIE — SIGNALS



BOOM CARPETS

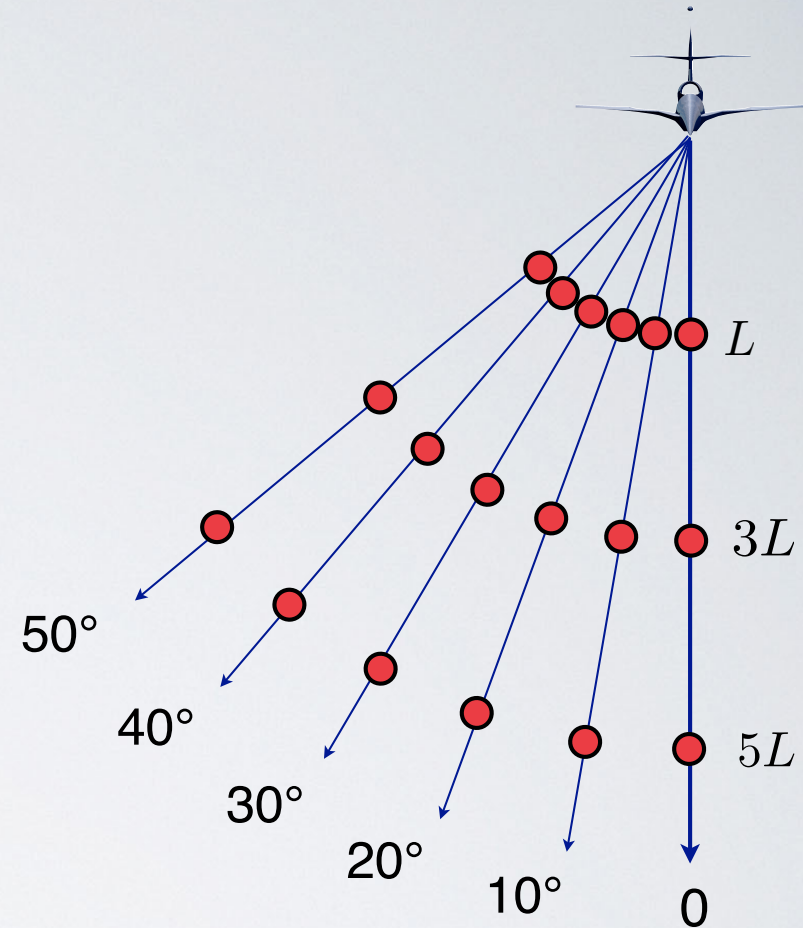
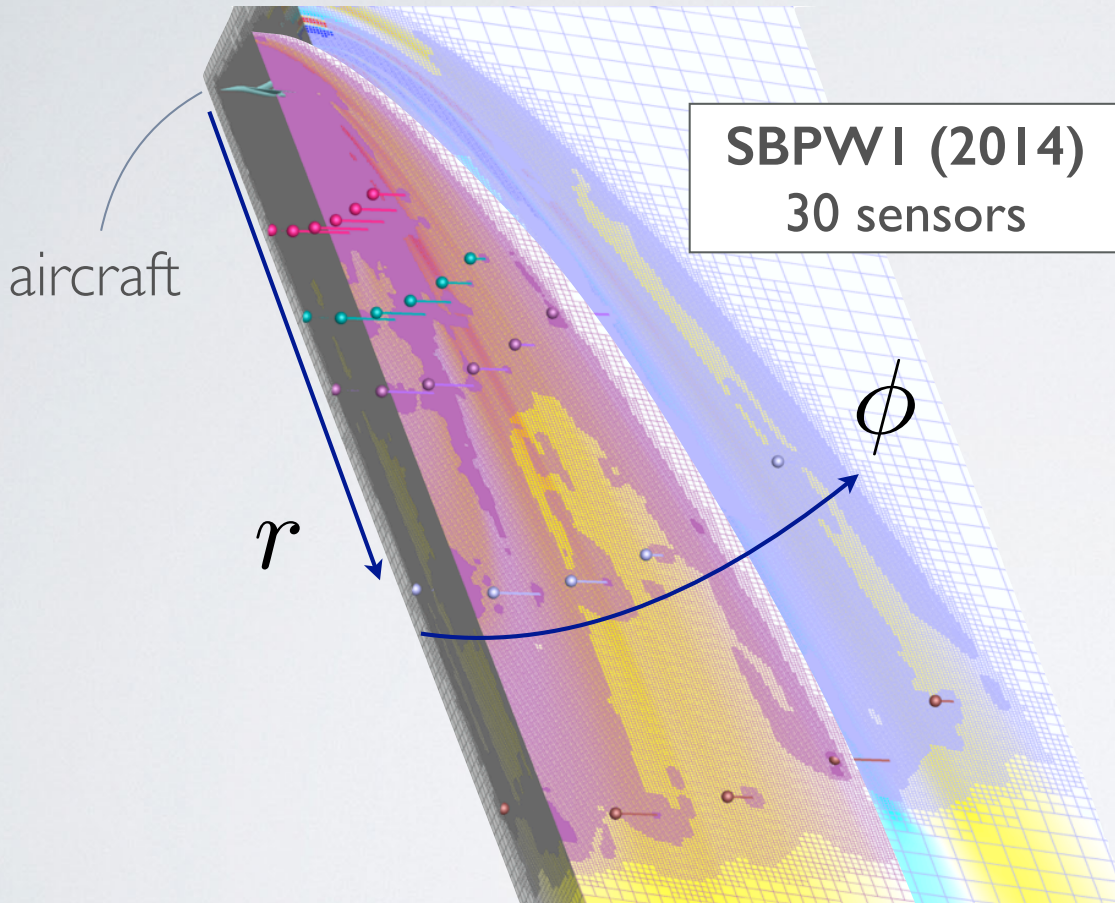


Boom Carpets



BOOM CARPETS WITH MONOLITHIC MESH

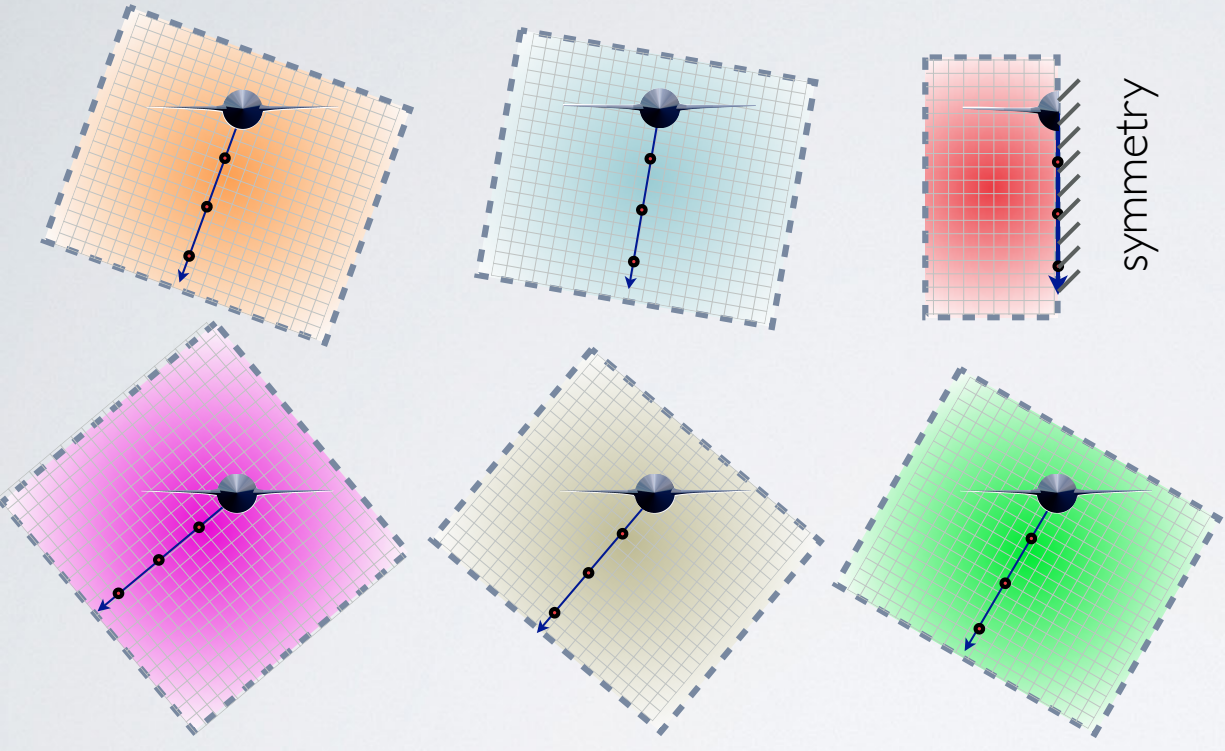
Compute entire carpet
in a single Cartesian mesh



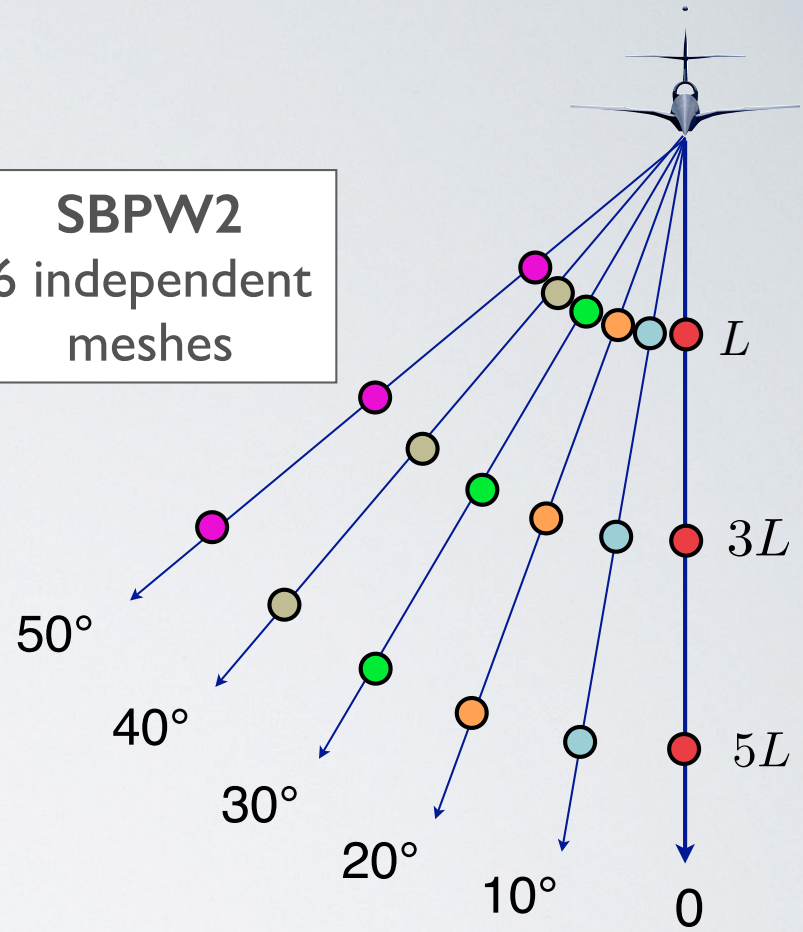
- ▶ Off-track angles are misaligned
 - ▶ Aspect ratio is constrained
- } **high cell-counts**

DECOMPOSING BOOM CARPETS

Use independent meshes
each rotated to off-track angle

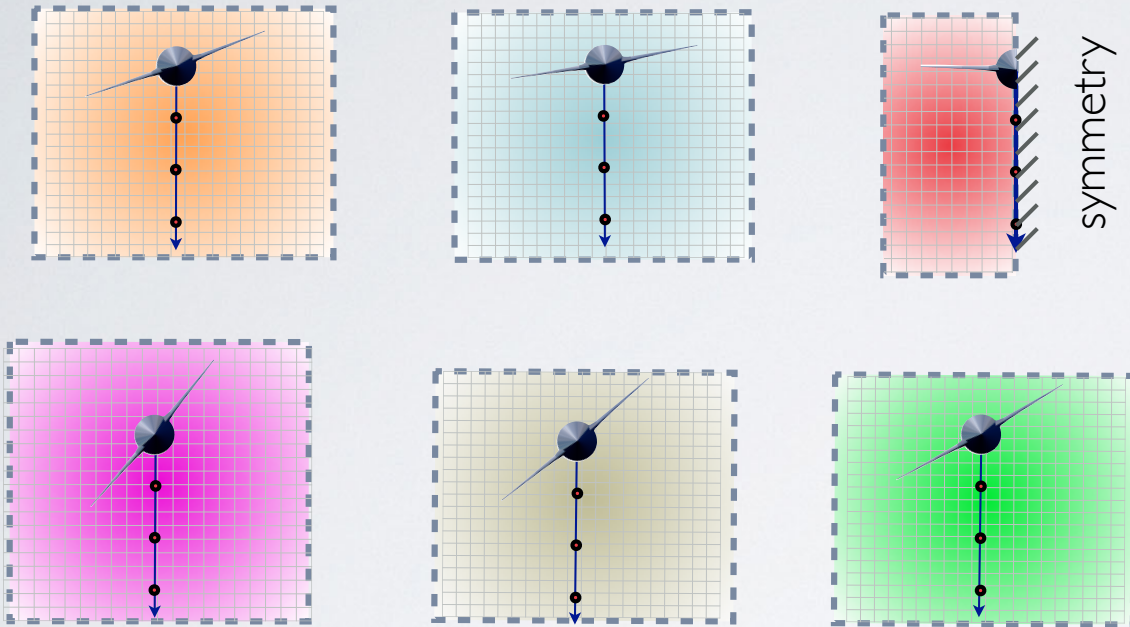


SBPW2
6 independent meshes

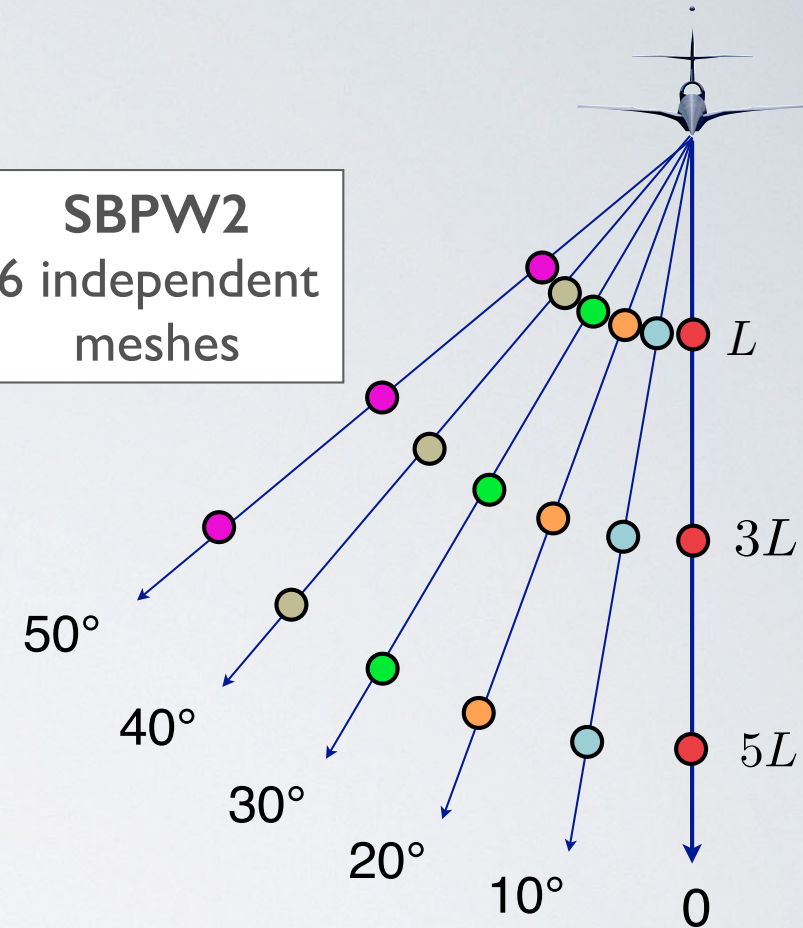


DECOMPOSING BOOM CARPETS

Use independent meshes
each rotated to off-track angle



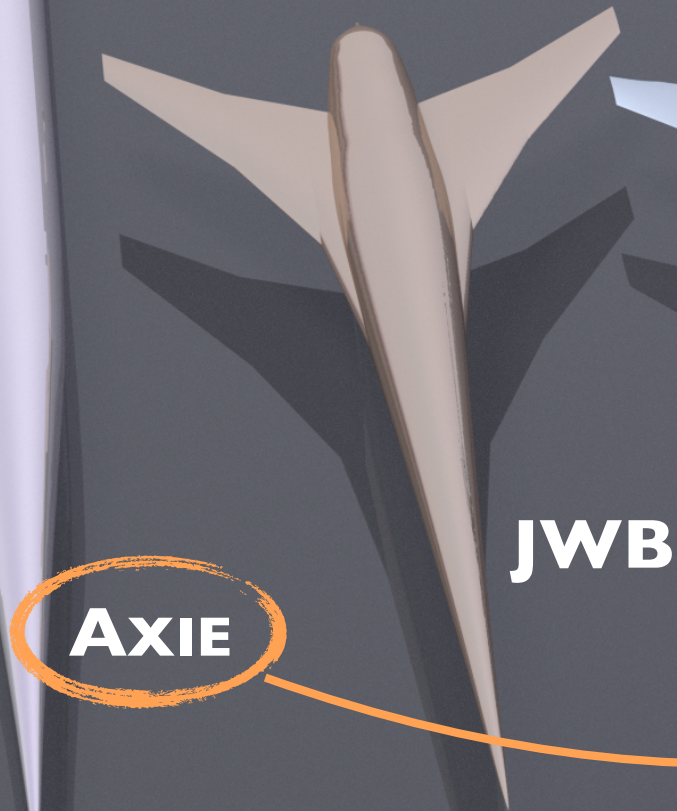
SBPW2
6 independent meshes



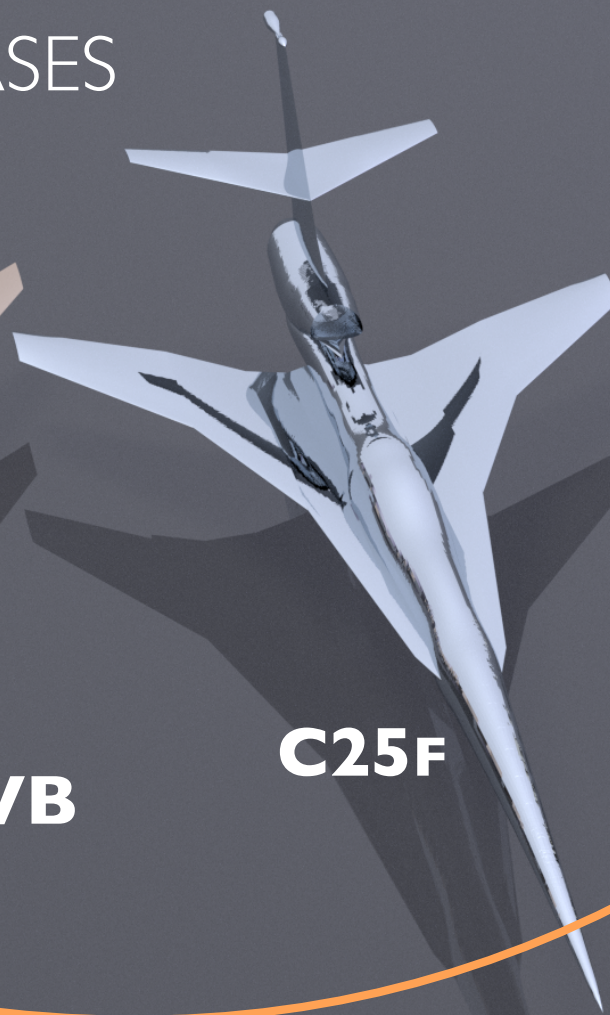
Splitting permits

- ▶ **azimuthal alignment**, which permits:
 - ▶ higher **stretching**
- ▶ Simultaneous computation of off-track angles in carpet

NEARFIELD CASES



JWB



ALL CASES:
MACH 1.6
Altitude: 15.76 km
(~52K feet)

CONCEPT 25D

POWERED VARIANT (**C25P**)

Flight Conditions

Mach 1.6

$\alpha = 3.375^\circ$

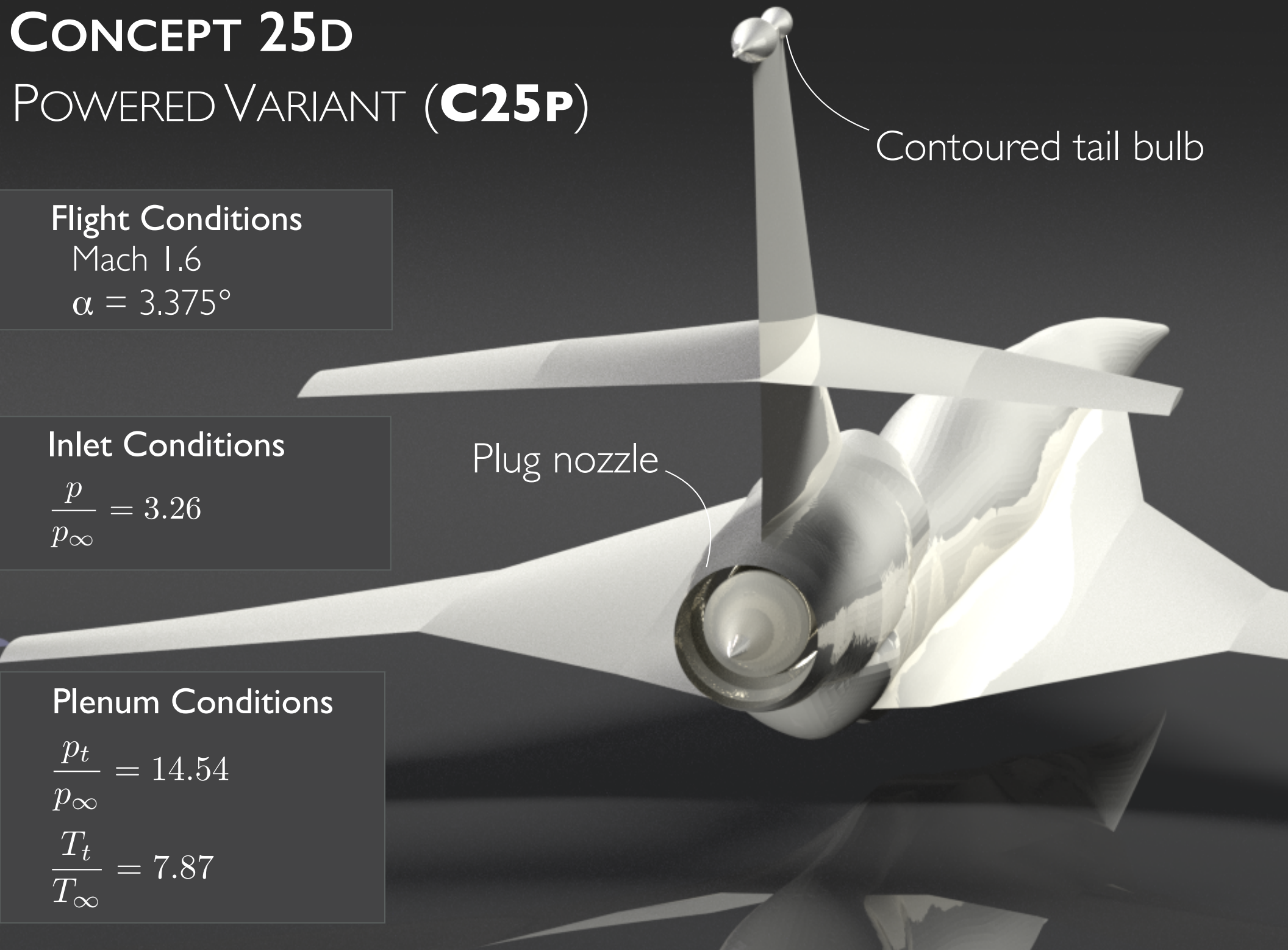
Inlet Conditions

$$\frac{p}{p_\infty} = 3.26$$

Plenum Conditions

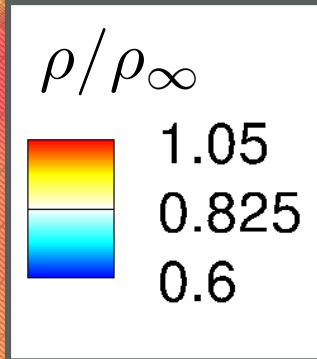
$$\frac{p_t}{p_\infty} = 14.54$$

$$\frac{T_t}{T_\infty} = 7.87$$

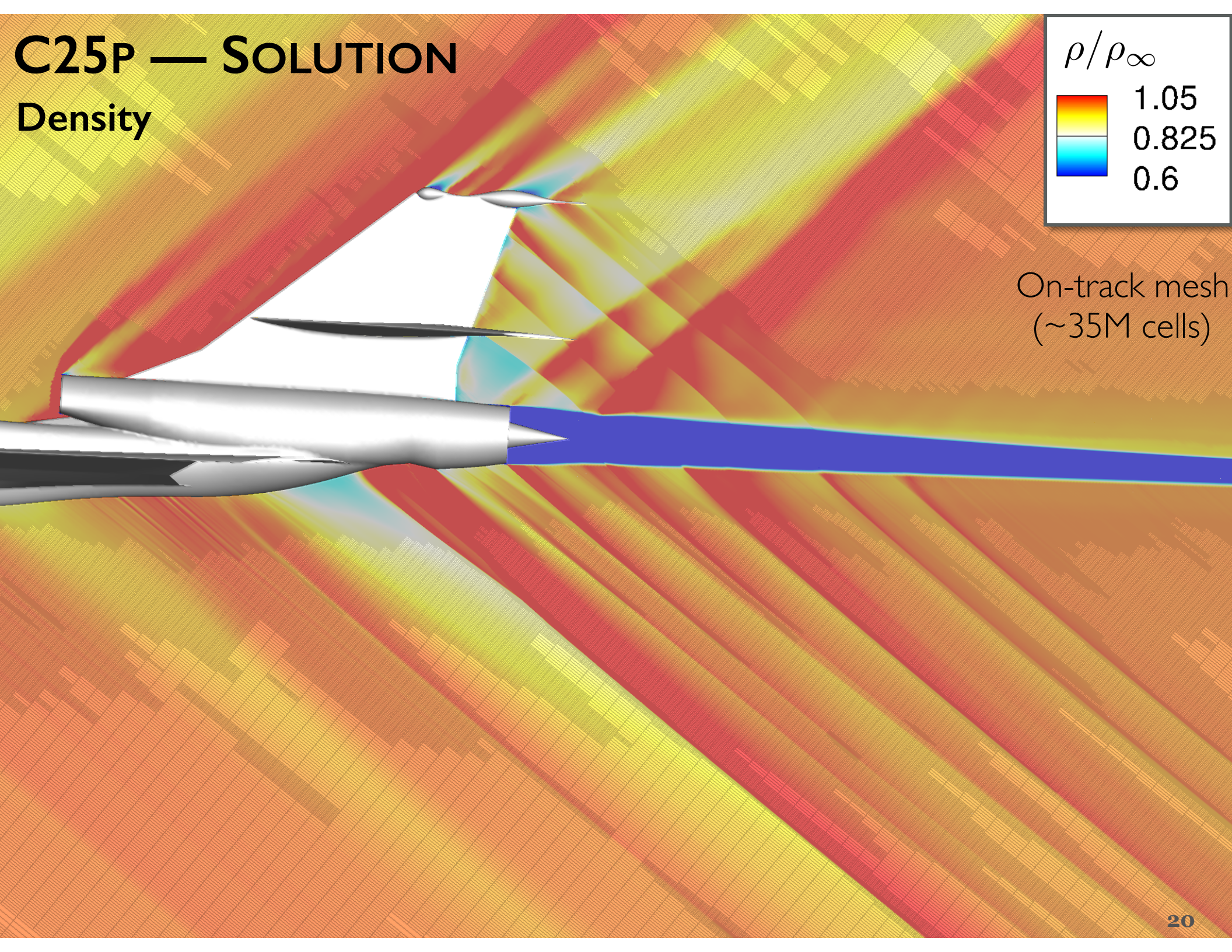


C25P — SOLUTION

Density

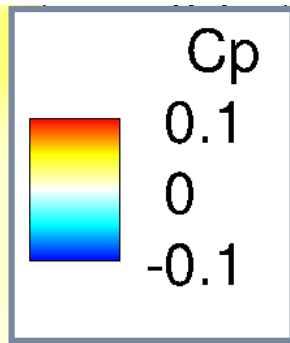


On-track mesh
(~35M cells)

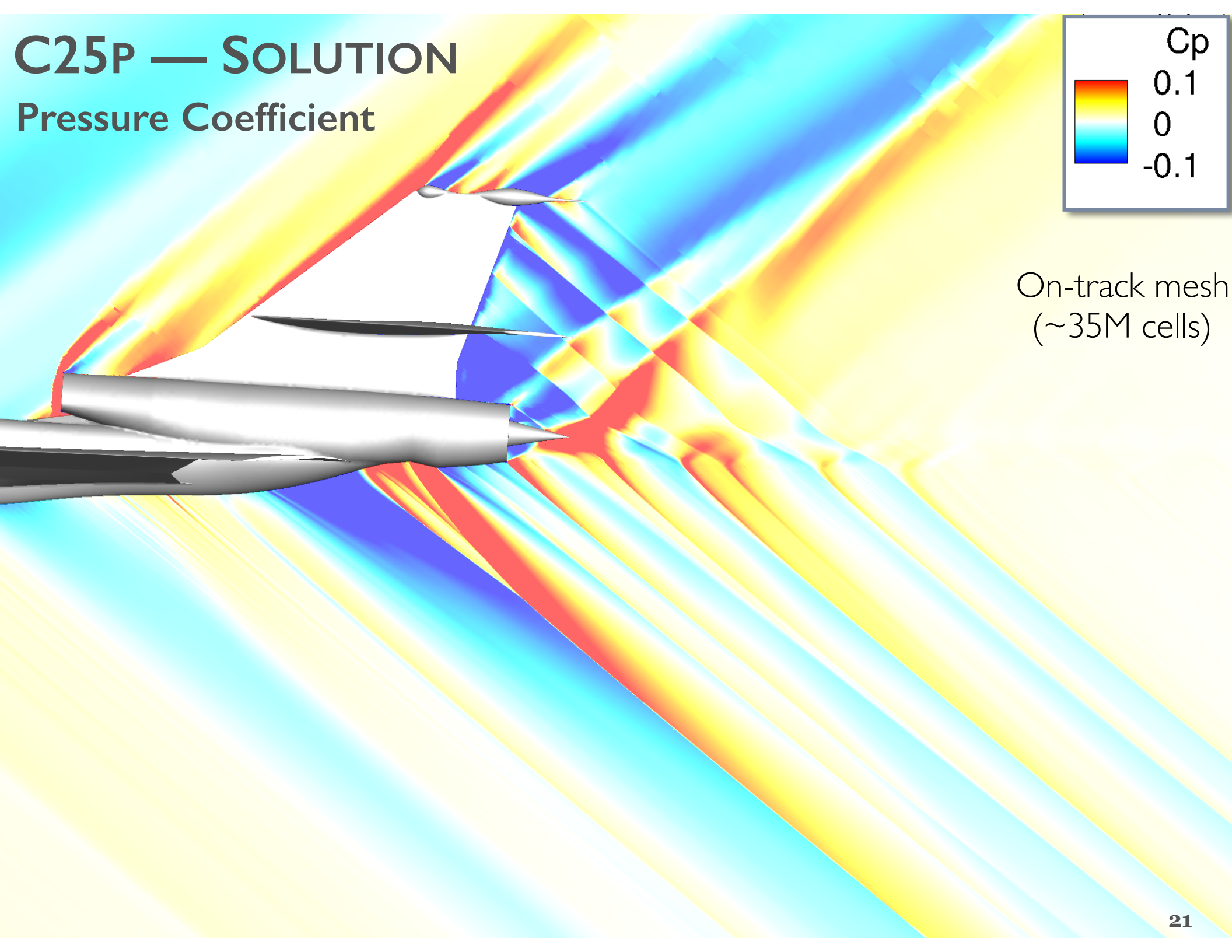


C25P — SOLUTION

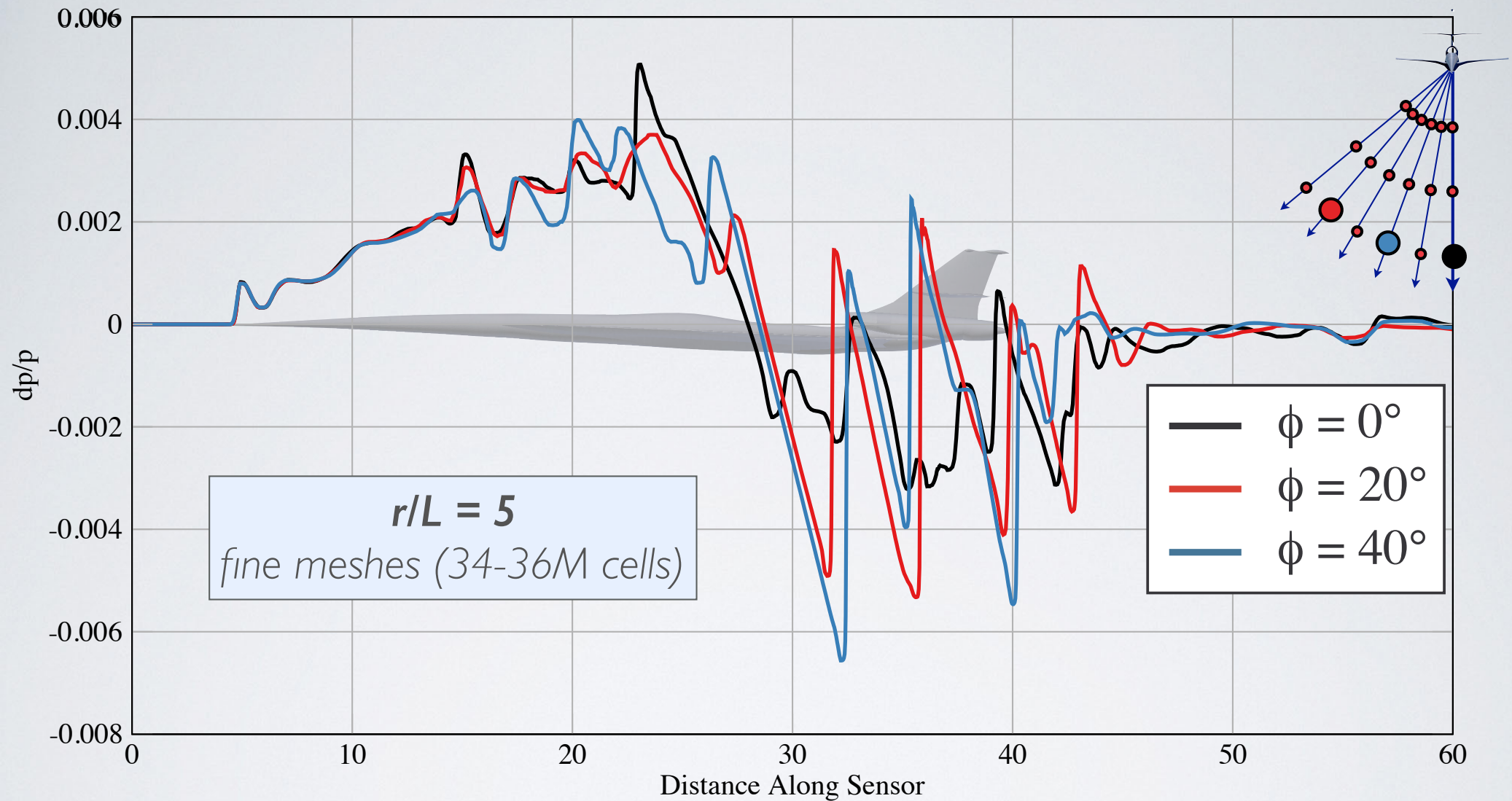
Pressure Coefficient



On-track mesh
(~35M cells)



C25P — SIGNATURES



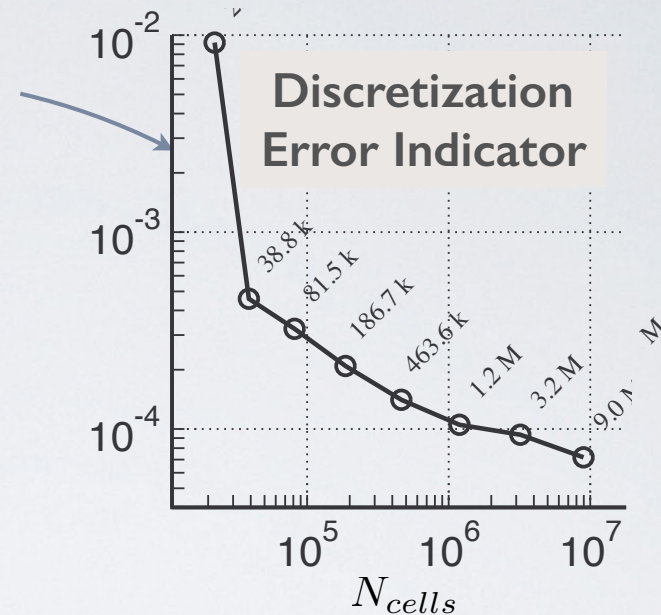
Each off-track angle — 35M cell mesh: 4hr 30min on 28 cores
Includes flow solution + all meshing, adjoint solutions, error estimation, etc.

ASSESSING MESH CONVERGENCE

Adjoint: Is the integrated functional converging asymptotically?

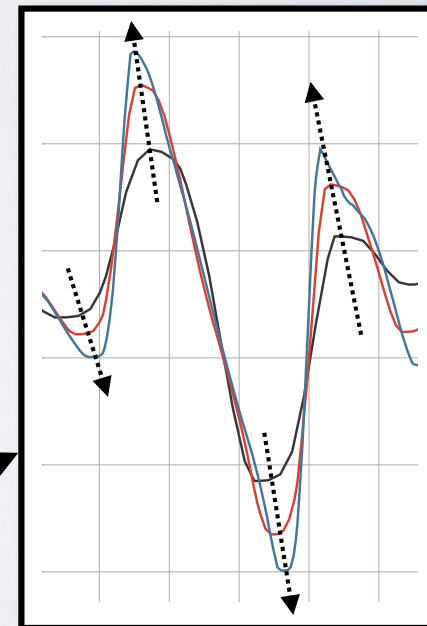
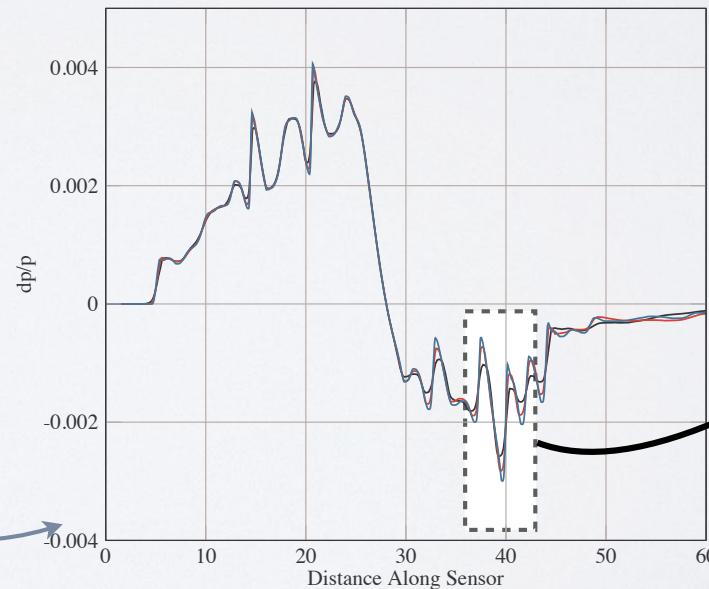
- ▶ Non-intuitive units on error

$$\mathcal{J}_r = \int_0^L w(\ell) \left(\frac{p(\ell) - p_\infty}{p_\infty} \right)^2 d\ell$$



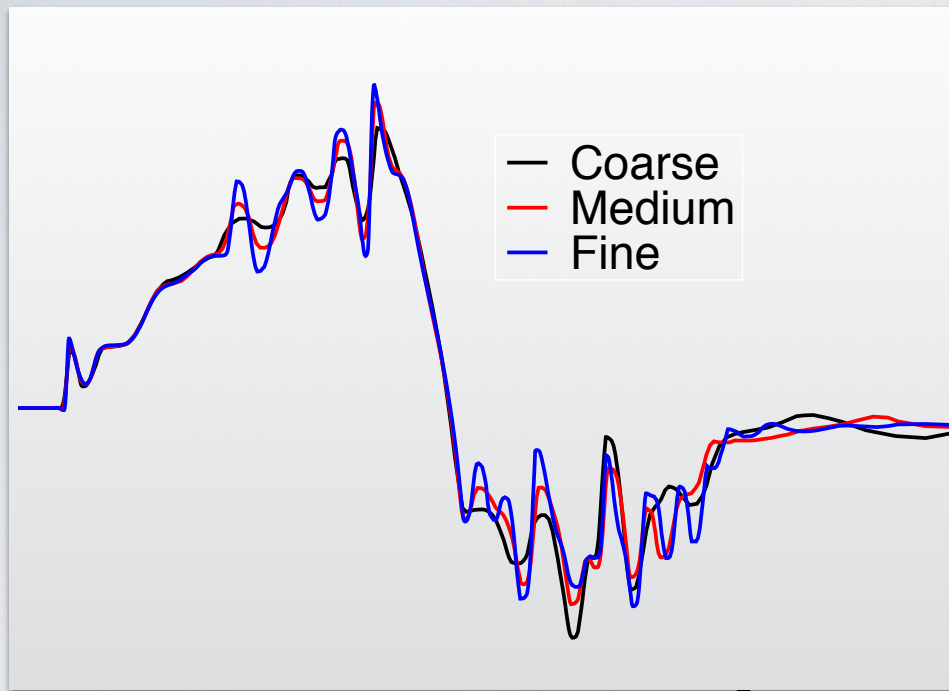
Qualitative: Are signal features converging with mesh refinement?

- ▶ Out of context, has no quantitative anchor, however:
- ▶ The signatures are the result of an error reducing process.



- Coarse (3M)
- Medium (9M)
- Fine (26M)

LOCAL ERROR ANALYSIS



Local Richardson extrapolation

- ▶ Incorporates estimate of global rate of convergence
- ▶ Reveals significant **local** variation in error and rate of convergence
- ▶ Can be used for any mesh refinement technique (not just adjoint-based)

Details: *AIAA Paper 2017-3255*

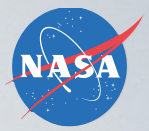


Figure 10. AXIE signature computed on fine grids plotted with discretization error estimates ($R = 5$).



a) AA, CA, CC, FA (shown), GA, HA, IA, JA.

Good convergence
everywhere, tight bounds
[8 participants]

(2017) Park and Nemec, "Nearfield Summary and Statistical Analysis of the Second AIAA Sonic Boom Prediction Workshop"

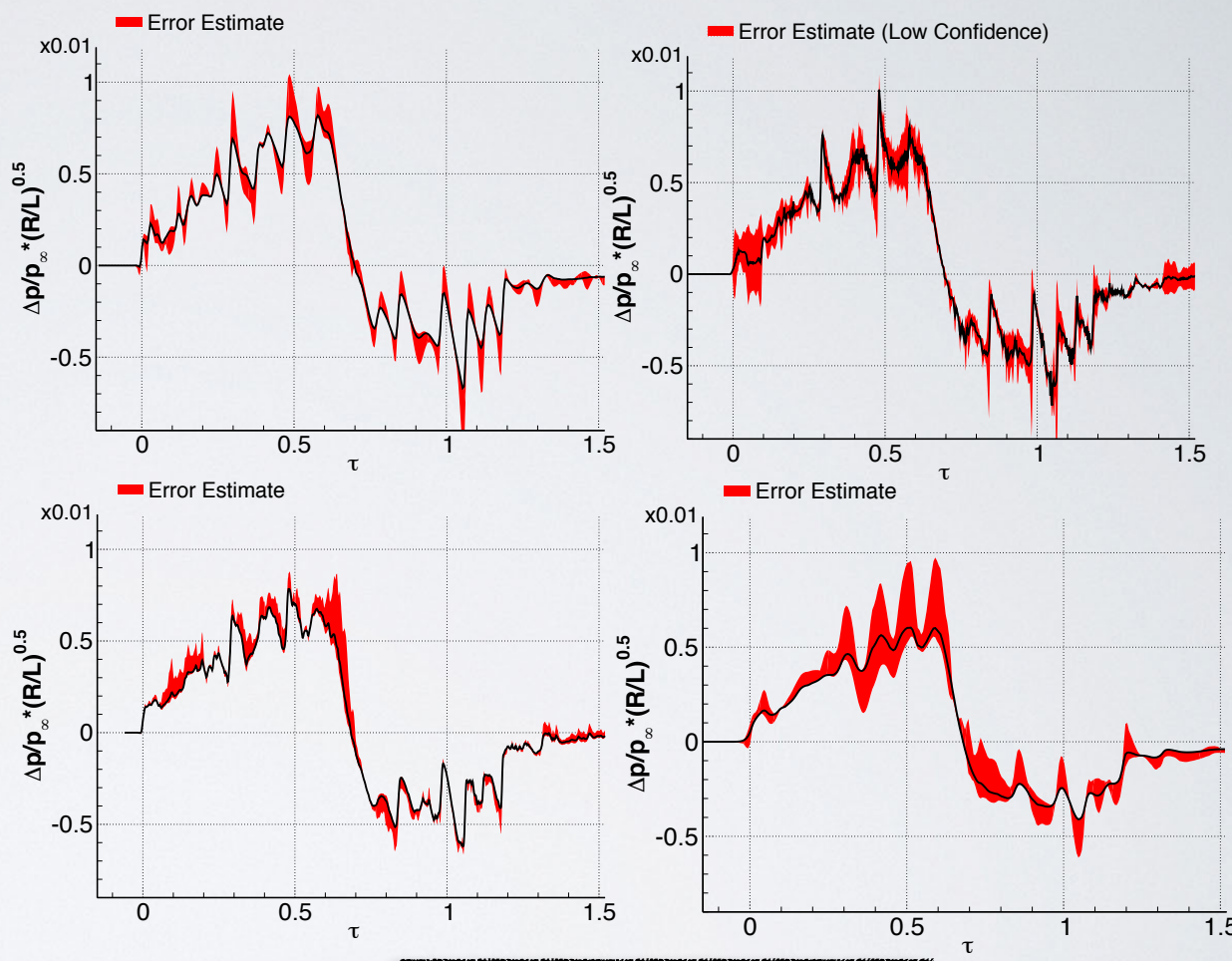


Figure 10. AXIE signature computed on fine grids plotted with discretization error estimates (R = 5).



a) AA, CA, CC, FA (shown), GA, HA, IA, JA.

Good convergence
everywhere, tight bounds
[8 participants]



Individual poorly converged results

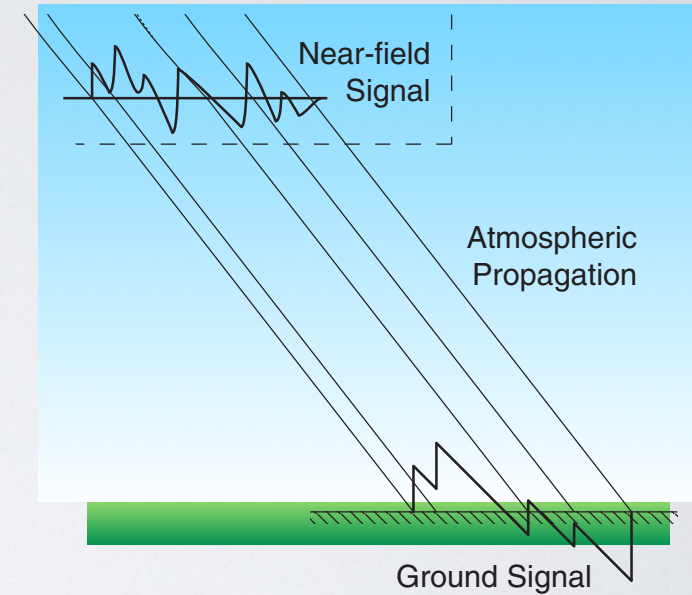
(2017) Park and Nemec, "Nearfield Summary and Statistical Analysis of the Second AIAA Sonic Boom Prediction Workshop"

✓ **Nearfield Workshop**

▶ **Propagation Workshop — sBOOM**

- Numerical approach
- Propagation Results

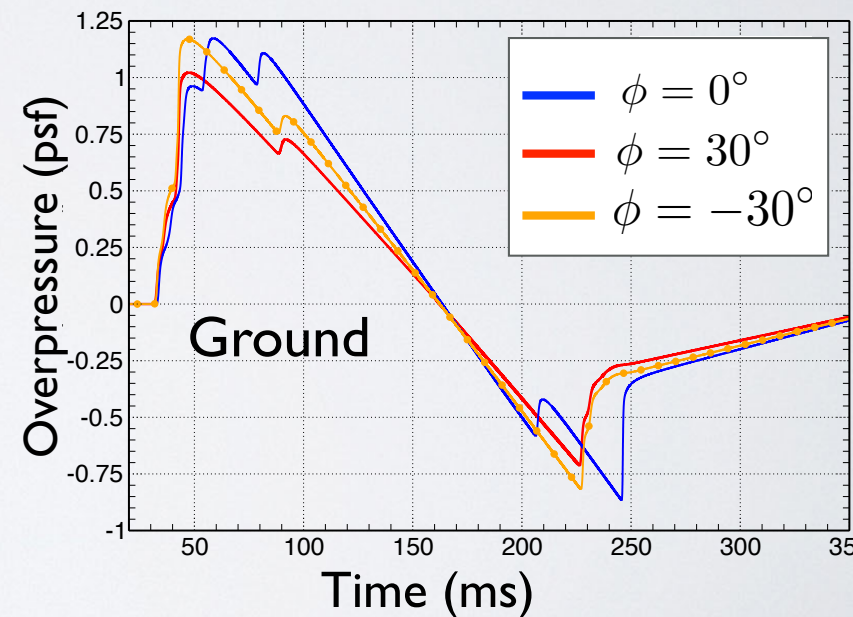
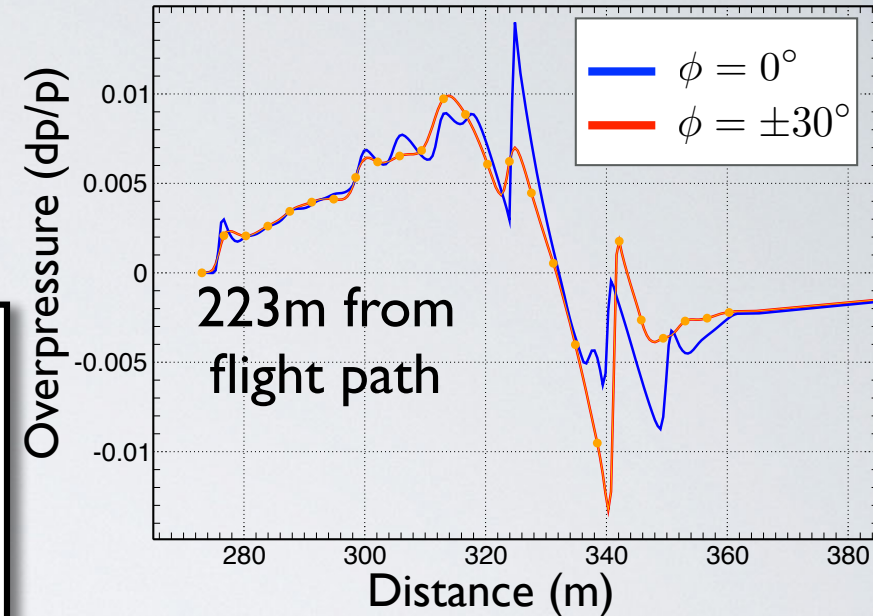
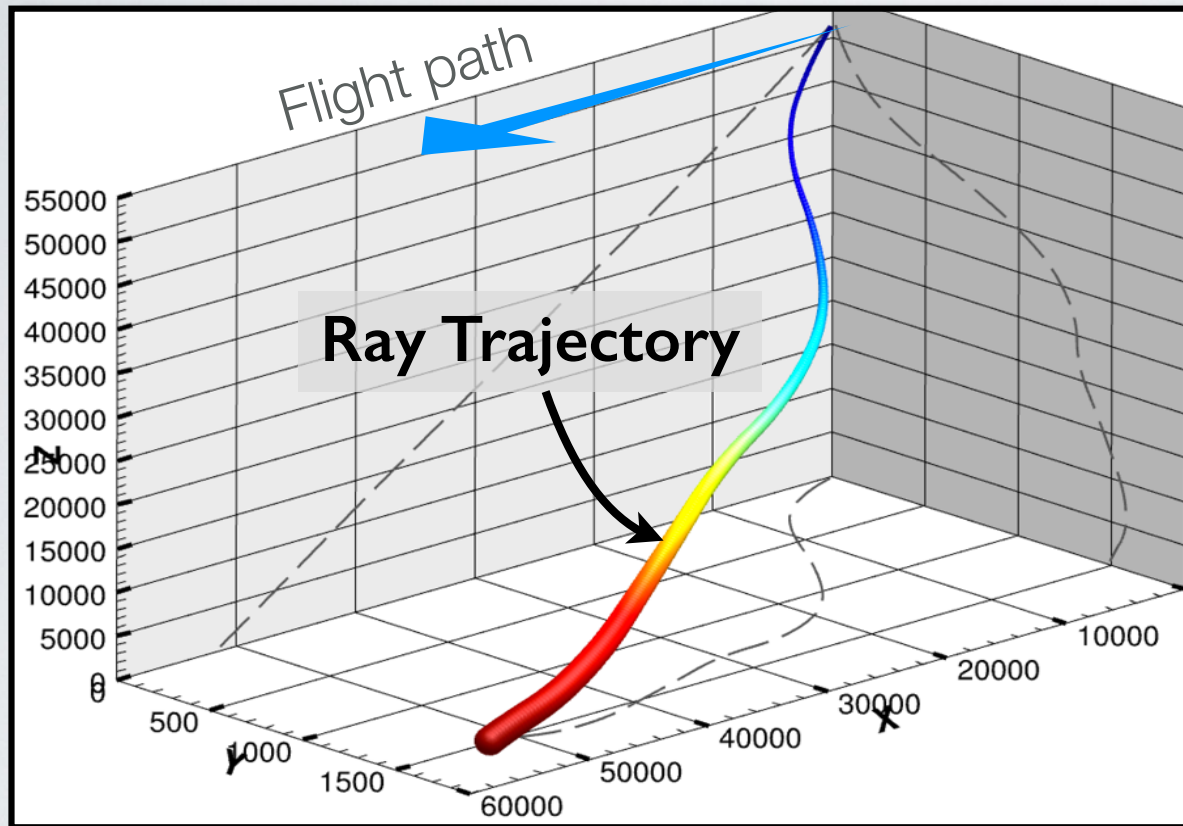
- Full Vehicle-to-Boom Simulation Path
- Conclusions



ATMOSPHERIC PROPAGATION WITH sBOOM

sBOOM

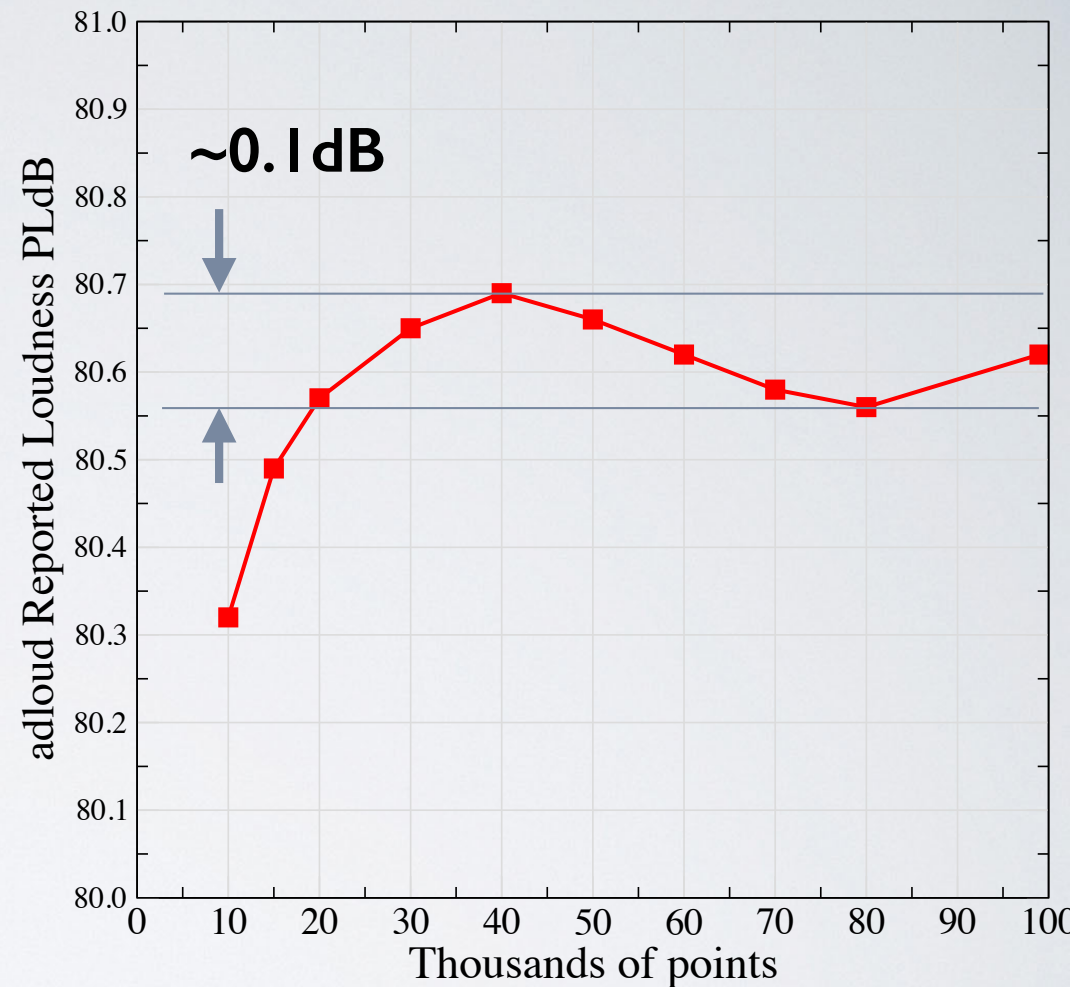
1. Ray-tracing
2. Quasi-1D, augmented Burgers' equation



(2011) Rallabhandi, "Advanced Sonic Boom Prediction Using the Augmented Burgers Equation"

ATMOSPHERIC PROPAGATION WITH SBOOM

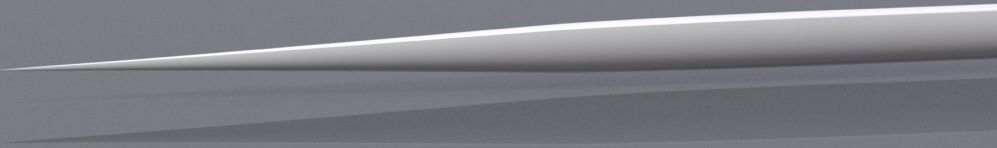
- ▶ **Discretization error**
Finite difference solution of PDE on uniform grid
- ▶ **Input error**
Input $\sim 100\times$ coarser than output
Oversampling introduces high freq.
- ▶ **Mesh refinement studies**
Numerical sources of error ~ 0.1 dB
(*cf. atmospheric variability of ~ 5 dB*)
But not clearly asymptotic



PROPAGATION CASES



AXIE



$L_{ref} = 43\text{m}$ (141 ft)

Conditions:

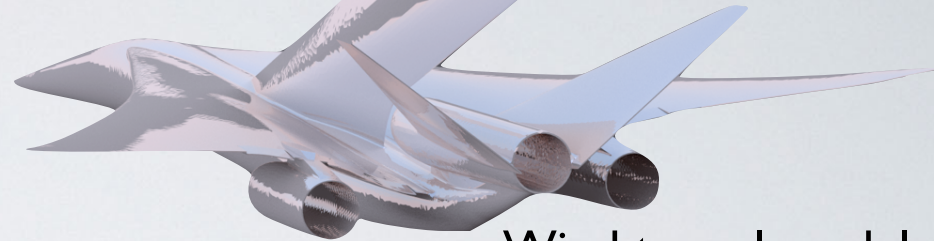
$$M_{\infty} = 1.6$$

Altitude = 15.8 km (~52K ft)

Profiles:

- ISO Standard Atmosphere
- ISO Std. Atm. with 70% humidity
- Hot day, coastal Virginia
- Hot dry day, Edwards AFB

LM-1021



Wind tunnel model
from SBPWI (2014)

$L_{ref} = 71\text{m}$ (233 ft)

Conditions:

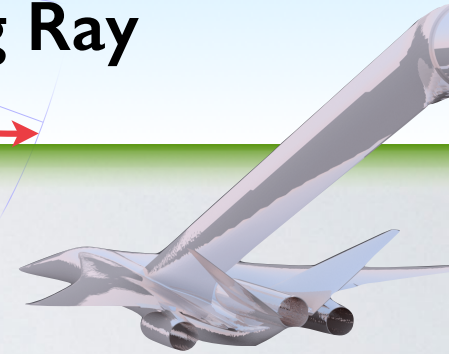
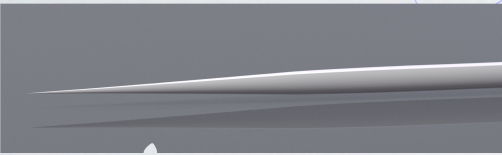
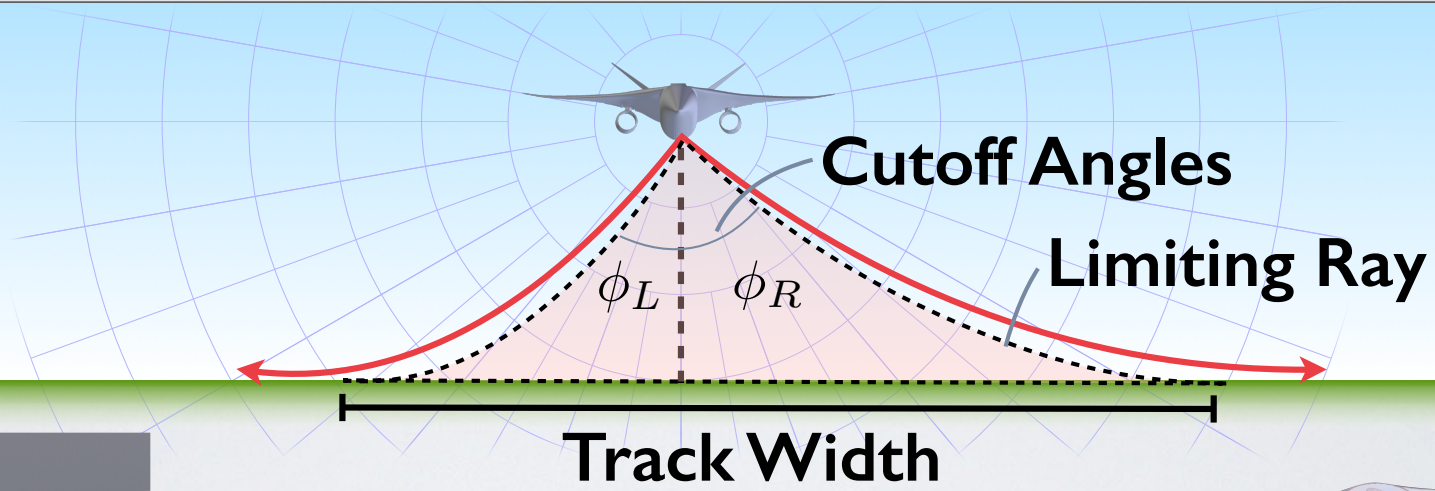
$$M_{\infty} = 1.6$$

Altitude = 16.7 km (~55K ft)

Profiles:

- ISO Standard Atmosphere
- ISO Std. Atm. with 70% humidity
- 2 consecutive winter days in Green Bay, WI

BOOM FOOTPRINT



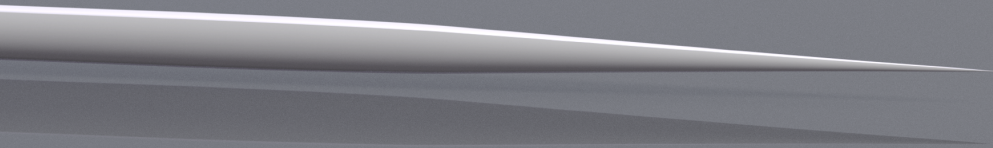
AXIE	Cutoff		Track Width
Std. Atm	$\pm 50^\circ$		69 km
Atm # 3	-53°	50°	85 km
Atm # 4	-44°	47°	72 km

LM-1021	Cutoff		Track Width
Std. Atm	$\pm 50^\circ$		71 km
Atm # 1	-74°	57°	87 km
Atm # 2	-59°	65°	111 km

LOUDNESS

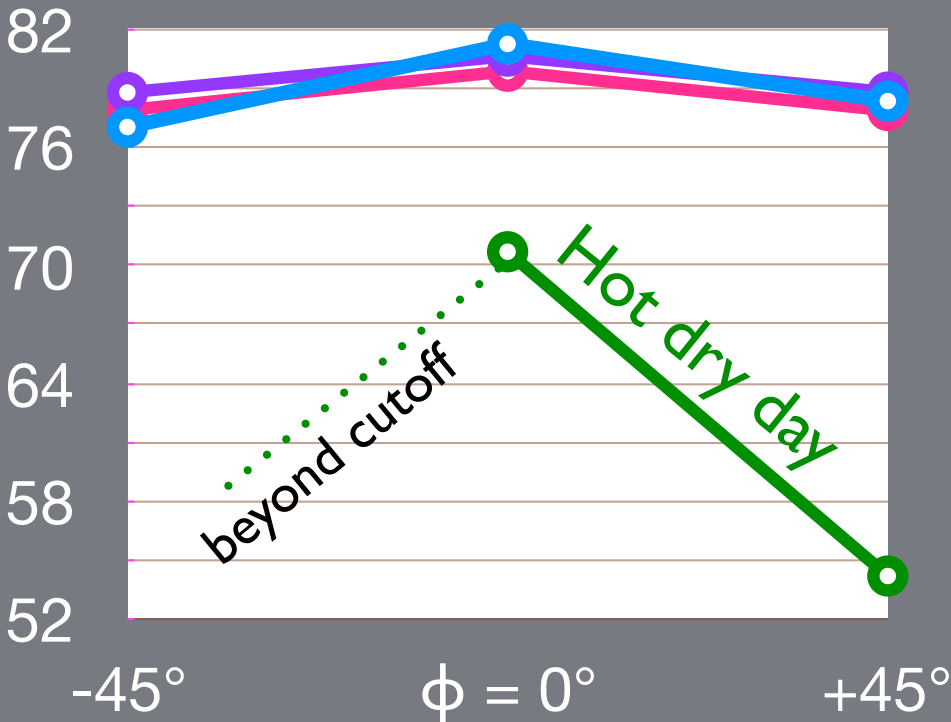


AXIE

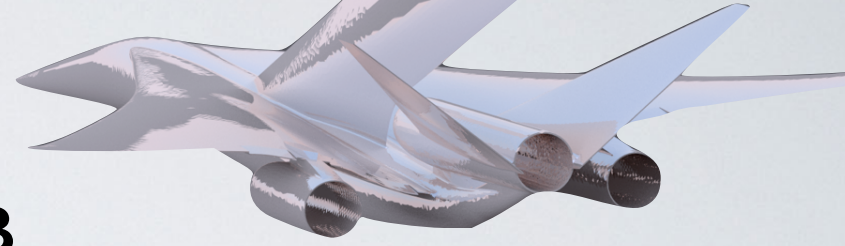


PLdB*

- Atm #3
- Std. Atm
- Atm #4
- Std. Atm+70%RH

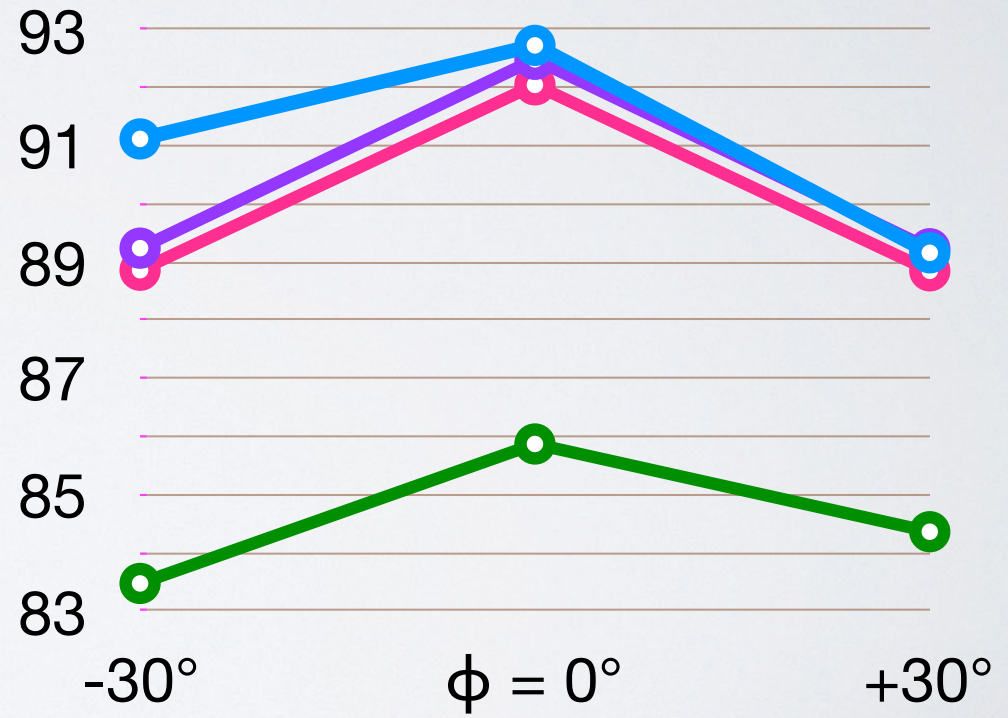


LM-1021



PLdB

- Atm #1
- Std. Atm
- Atm #2
- Std. Atm+70%RH



*(1991) Shepherd & Sullivan, "A Loudness Calculation Procedure Applied to Shaped Sonic Booms"

✓ **Nearfield Workshop**

✓ **Propagation Workshop — sBOOM**

▶ **Full Vehicle-to-Boom Simulation Path**

- Propagate nearfield CFD signatures through standard atmosphere
- Overall convergence and accuracy

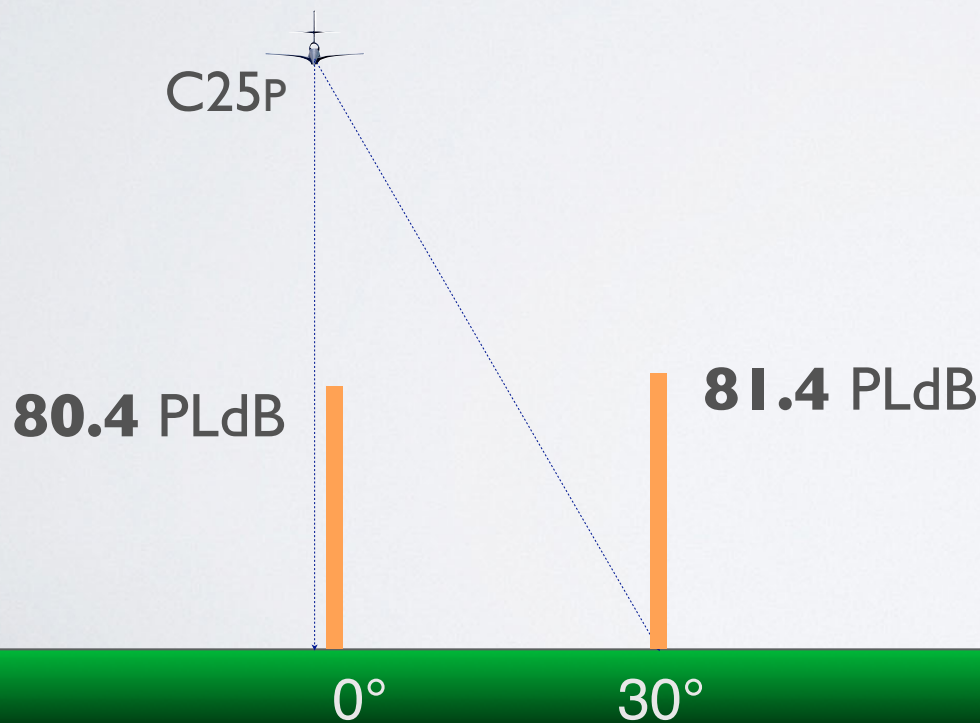
• **Conclusions**

NEARFIELD + PROPAGATION

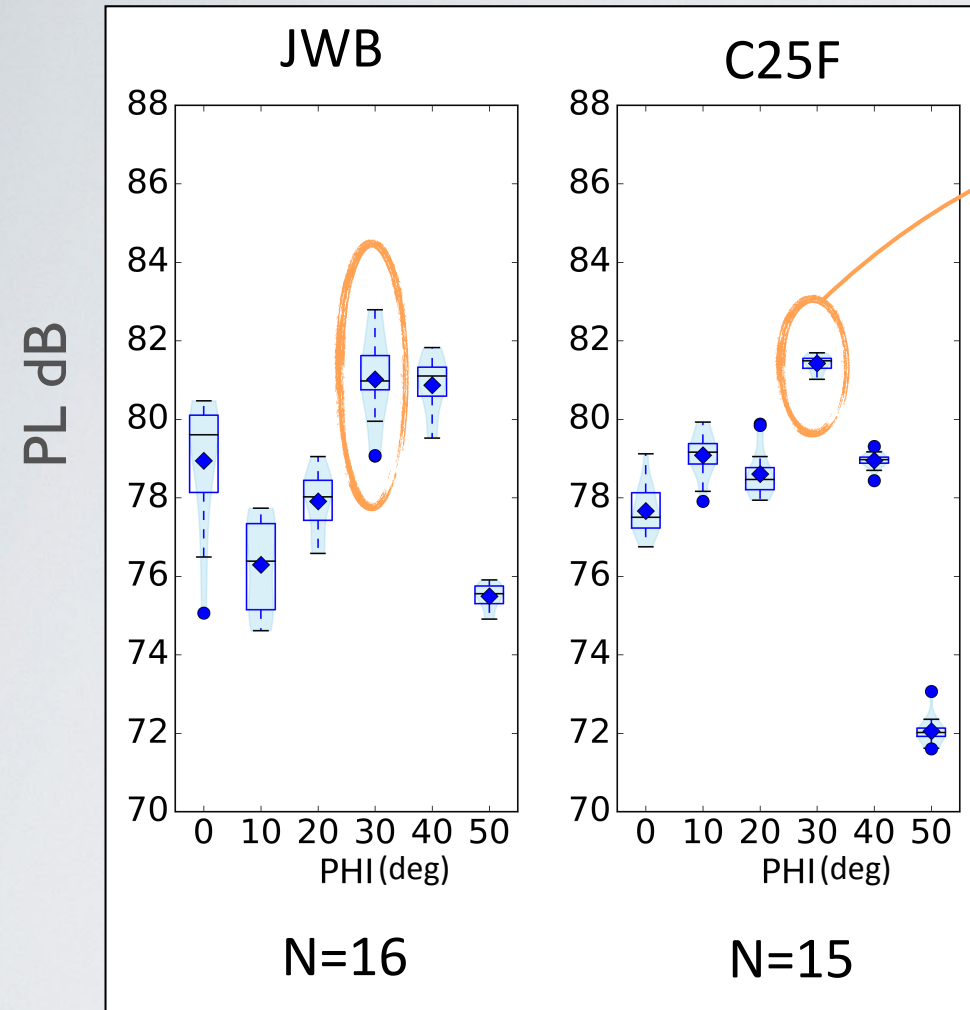
Perceived loudness (PLdB)

from $r/L=5$ on fine CFD mesh

Case	$\Phi = 0^\circ$	$\Phi = 10^\circ$	$\Phi = 20^\circ$	$\Phi = 30^\circ$	$\Phi = 40^\circ$	$\Phi = 50^\circ$
AXIE	78.1	—	—	—	—	—
JWB	79.5	76.5	78.2	82.2	81.6	76.6
C25F	78.1	80.4	80.1	82.2	80.1	73.3
C25P	80.4	81.3	78.3	81.4	78.7	73.3



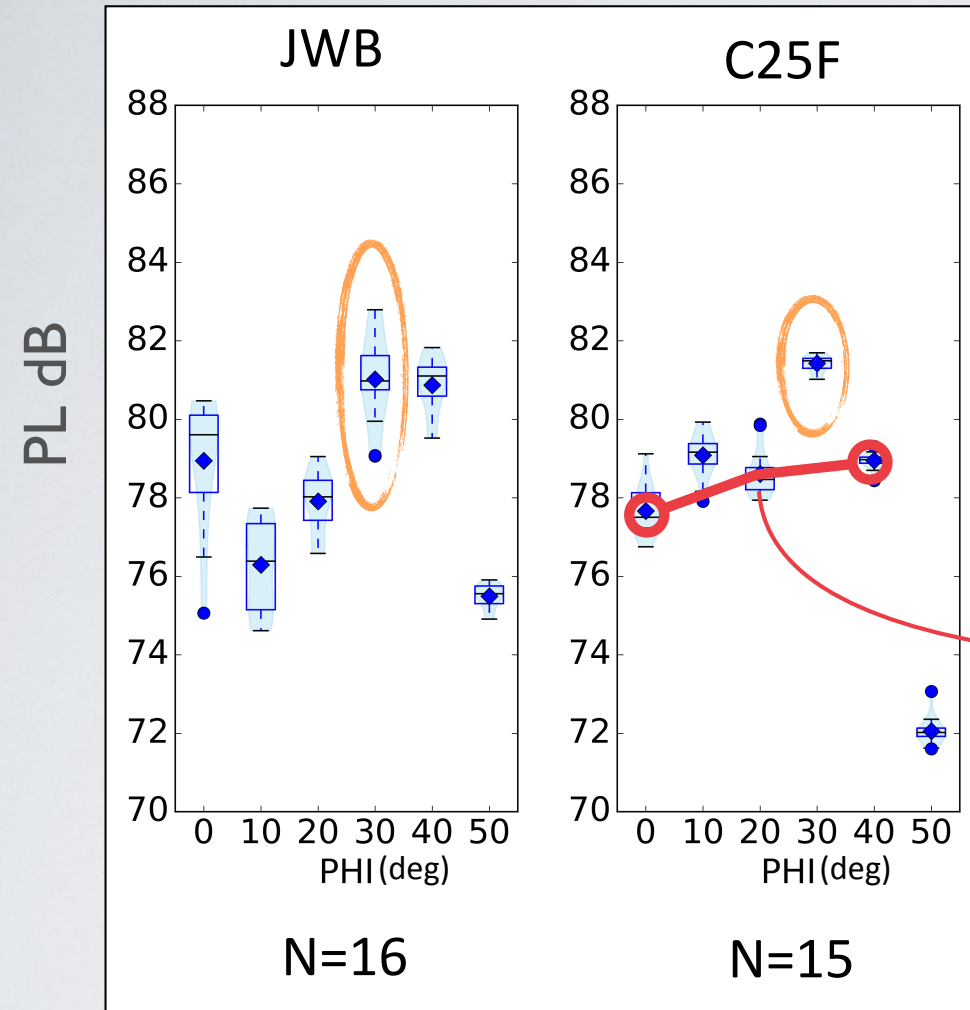
COMPARISON



Off-track boom is not just relevant, but critical!

(2017) Park and Nemeec, *“Nearfield Summary and Statistical Analysis of the Second AIAA Sonic Boom Prediction Workshop”*

COMPARISON



Off-track boom is not just relevant, but critical!

A coarser carpet discretization ($\Delta\Phi=20^\circ$) would have under-predicted the worst boom by ~ 3 dB!

(2017) Park and Nemeć, “*Nearfield Summary and Statistical Analysis of the Second AIAA Sonic Boom Prediction Workshop*”

CFD MESH CONVERGENCE OF LOUDNESS

Perceived loudness (PLdB)

from $r/L=5$ on fine CFD mesh

Case	$\Phi = 0^\circ$	$\Phi = 10^\circ$	$\Phi = 20^\circ$	$\Phi = 30^\circ$	$\Phi = 40^\circ$	$\Phi = 50^\circ$
AXIE	78.1 (0.4)	—	—	—	—	—
JWB	79.5 (0.6)	76.5 (0.7)	78.2 (0.4)	82.2 (1.5)	81.6 (0.1)	76.6 (0.5)
C25F	78.1 (0.8)	80.4 (0.6)	80.1 (0.1)	82.2 (0.8)	80.1 (0.6)	73.3 (0.0)
C25P	80.4 (0.5)	81.3 (0.5)	78.3 (0.3)	81.4 (0.6)	78.7 (0.4)	73.3 (1.6)

$\Delta PLdB$ from coarse to fine CFD mesh

- ▶ Typically < 1 dB change from coarse to fine CFD mesh (max 1.6 dB)
- ▶ Most do not demonstrate **asymptotic** convergence.
- ▶ Summary results indicate similar behavior across many codes

$$\mathcal{J}_r = \int_0^L w(\ell) \left(\frac{p(\ell) - p_\infty}{p_\infty} \right)^2 d\ell$$

used as a convenient **surrogate** for loudness

- ▶ **Improving CFD/Propagation Coupling**
 - ▶ Better understanding the CFD meshing requirements
 - ▶ Using noise sensitivities to guide CFD mesh adaptation (direct adaptation to noise vs. surrogate functionals)
 - ▶ Better interpolation/transfer of signatures

- ▶ **Physics**
 - ▶ Wake unsteadiness
 - ▶ Maneuver, elastic effects, control surfaces
 - ▶ Propagation — secondary booms, reflections

HIGHLIGHTS

Nearfield with Cart3D

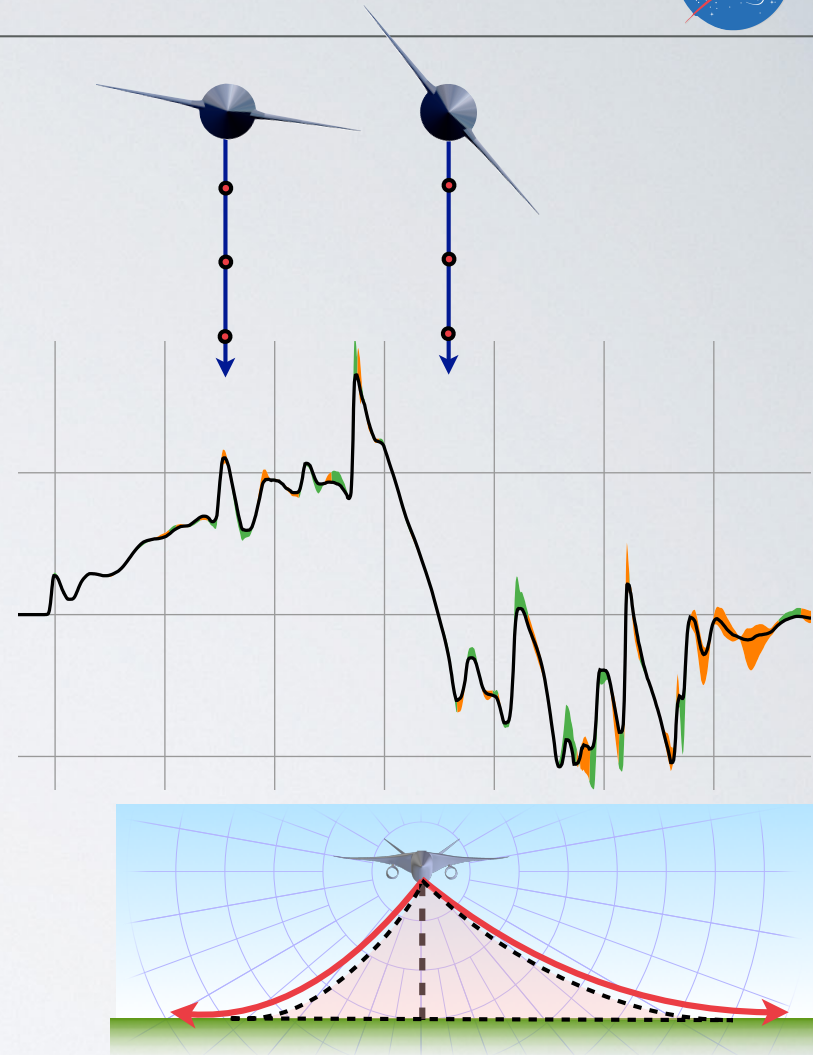
- ▶ Improved efficiency by carpet splitting, azimuthal alignment, and stretching
- ▶ Method for assessing local signature mesh convergence *[scripts available]*

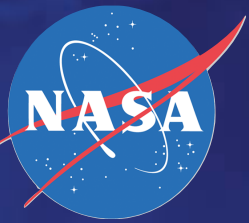
Propagation with sBOOM

- ▶ Major atmospheric variability: 2-5 dB typical, 10-20 dB in extreme cases.
- ▶ With cross-wind, **75° off-track** can hit ground, **track widths widen by 50%**

Full Boom Simulation Path

- ▶ Need to better understand asymptotic convergence of noise





QUESTIONS?



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